

1 **Title:** A new energetics model for the assessment of the power-duration relationship  
2 during over-ground running

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1 **Abstract**

2 We evaluated the reliability of an over-ground running three-minute all-out test (3MT)  
3 and compared this to traditional multiple-visit testing to determine the critical speed  
4 (CS) and distance >CS ( $D'$ ). Using a novel energetics model during the 3MT, critical  
5 power (CP) and work >CP ( $W'$ ) were also evaluated for reliability and compared to the  
6 multiple-visit tests. Over-ground running speed was measured using Global  
7 Positioning Systems during fixed-speed trials on a 400 m track to exhaustion, at four  
8 intensities corresponding to: i) maximal oxygen uptake ( $\dot{V}O_{2max}$ ) ( $V_{max}$ ), ii) 110%  $\dot{V}O_{2max}$   
9 (110% $V_{max}$ ), iii)  $\Delta 70\%$  (i.e. 70% of the difference between gas exchange threshold and  
10  $V_{max}$ ) and iv)  $\Delta 85\%$ . The participants subsequently performed the 3MT across two  
11 days to determine its reliability. There were no differences between the multiple-visit  
12 testing and the 3MT for CS ( $P = 0.328$ ) and  $D'$  ( $P = 0.919$ ); however, CP ( $P = 0.02$ )  
13 and  $W'$  ( $P < 0.001$ ) were higher in the 3MT. The reliability of the 3MT was stable ( $P >$   
14  $0.05$ ) between trials for all variables, with coefficient of variation ranging from 2.0 to  
15 8.1%. The current over-ground energetics model can reliably estimate CP and  $W'$   
16 based on GPS speed data during the 3MT, which supports its use for most athletic  
17 training and monitoring purposes. The reliability of the over-ground running 3MT for  
18 power- and speed-related indices was sufficient to detect typical training adaptations;  
19 however, it may overestimate CP (~ 25 W) and  $W'$  (~ 7 kJ) compared to multiple-visit  
20 tests.

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22 **Key words:** Critical power; critical speed; energetics; endurance.

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## 1 Introduction

2 The slope of the linear relationship between distance and time (critical speed; CS) and  
3 the y-intercept ( $D'$ ) characterise the speed-duration model (Hughson, Orok, & Staudt,  
4 1984). The CS is indicative of the highest rate of oxidative metabolism, below which  
5 physiological equilibrium can be maintained and beyond which progressive deviation  
6 from homeostasis occurs, resulting in exercise intolerance (Poole, Burnley, Vanhatalo,  
7 Rossiter, & Jones, 2016). The  $D'$  is the finite distance that can be performed above  
8 CS (Jones, Vanhatalo, Burnley, Morton, & Poole, 2010). Among athletes whose mode  
9 of locomotion is over-ground running, these parameters have been used to profile  
10 endurance capacity (Kramer, Clark, Jamnick, Strom, & Pettitt, 2018; Kramer, Watson,  
11 Du Randt, & Pettitt, 2019), monitor responses to training interventions (Clark, West,  
12 Reynolds, Murray, & Pettitt, 2013; Galbraith, Hopker, Cardinale, Cunniffe, & Passfield,  
13 2014) and determine optimal race or training strategies (Pettitt, 2016; Saari, Dicks,  
14 Hartman, & Pettitt, 2019). These applications have been typically based upon  
15 estimations of the speed-duration relationship using single-visit tests, of varying  
16 composition, in an outdoor setting. The three-minute all-out test (3MT) is the most  
17 common among these, typically performed as a maximal sprint effort around an  
18 athletics track with no knowledge of elapsed time to discourage pacing (Clark et al.,  
19 2013; Kramer et al., 2018; 2019; Pettitt, Jamnick, & Clark, 2012; Saari et al., 2019).  
20 Estimations of CS and  $D'$  from the 3MT compare closely to the traditional multiple-visit  
21 testing model, based on both treadmill (Broxterman, Ade, Poole, Harms, & Barstow,  
22 2013) and over-ground running modalities (de Aguiar et al., 2018).

23

24 The speed-duration relationship has historically been modelled using the  
25 performances of endurance athletes (Hughson et al., 1984), who compete at constant  
26 speeds in more predictable environments. More recently, its use among athletes  
27 competing in sports that are intermittent in nature, such as the majority of team sports,  
28 has been considered (Galbraith, Hopker, & Passfield, 2015; Jones & Vanhatalo, 2017;  
29 Saari et al., 2019). Team sports typically involve high-intensity bouts, interspersed by  
30 rest or periods of low-intensity activity; this in turn leads to frequent surges above and  
31 below the CS, the boundary demarcating the heavy and severe exercise intensity  
32 domains (Jones et al. 2010). Whilst there are many practical applications of the speed-

1 duration model to team sport athletes, such as assessment of training adaptation  
2 (Clark et al., 2013; Kramer et al., 2018), the use of speed to quantify the physiological  
3 demands of team sports appears to be limited (Gray, Shorter, Cummins, Murphy, &  
4 Waldron, 2018). The intermittent nature of team sports involve frequent acceleration,  
5 deceleration and changes in speed, leading to a de-coupling of the relationship  
6 between energetic demand and running speed (Polglaze et al., 2018). Consequently,  
7 the speed-duration relationship may be limited in classifying exercise intensity. This  
8 could have major implications for the accurate monitoring of training load in team  
9 sports players. For example, high-intensity (i.e. energy demanding) movements in  
10 team sports often occur at low-speed (Gray et al., 2018; Osgnach, Poser, Bernardini,  
11 Rinaldo, & di Prampero, 2010). The energy cost of running is elevated by increasing  
12 both absolute speed and its rate of change (Buglione & di Prampero, 2013). This has  
13 been recently attributed to greater mechanical demands of non-constant speed  
14 running, such as deceleration, acceleration and changing direction (Zamparo et al.,  
15 2019). Therefore, the suggested application of the speed-duration (rather than power-  
16 duration) model to intermittent exercise (Galbraith et al., 2015; Jones & Vanhatalo,  
17 2017) would be unable to capture all energy-demanding aspects of exercise,  
18 particularly at low speeds, resulting in poorer estimations of exercise tolerance.

19

20 To the authors' knowledge, there has been no investigation of the power-duration  
21 relationship during over-ground running. Our recent development of a new over-  
22 ground mechanical power model could, therefore, be applied to facilitate  
23 characterisation of the power-duration model during over-ground running in team  
24 sports athletes (Gray et al., 2018; Gray, Andrews, Waldron, & Jenkins, 2020). Using  
25 principles from work-energy theorem, this model algebraically summates positive and  
26 negative external work done across body segments using running velocity, alongside  
27 known participant characteristics and environmental conditions (Gray et al., 2020).  
28 Since work done is explained by a combination of many energy-demanding processes,  
29 such as acceleration of the centre of mass (CoM) and movement of the limbs  
30 (Zamparo et al., 2019), this model considers factors other than constant horizontal  
31 speed achieved by an athlete, better quantifying the demands of intermittent  
32 movement. Thus, modelling the power-duration relationship would be more suitable  
33 than the speed-duration relationship for monitoring intermittent performance.

1 However, understanding of the reliability and validity of over-ground power modelling  
2 and its utilisation for determining parameters of the power-duration relationship (critical  
3 power; CP and the finite work > CP;  $W'$ ) are required prior to further application.  
4 Therefore, the aim of the current study was to compare a single visit over-ground  
5 running 3MT to traditional multiple-visit procedures to determine parameters of the  
6 over-ground speed-duration (CS and  $D'$ ) and over-ground power-duration (CP and  
7  $W'$ ) models. Finally, the test re-test reliability of the 3MT was evaluated for both speed-  
8 and power-based parameters.

9

## 10 **Methods**

### 11 ***Participants***

12 Following institutional ethical approval, nine healthy male participants (age =  $24 \pm 3$   
13 years; body mass =  $70.8 \pm 6.0$  kg; stature =  $1.75 \pm 0.03$  m; maximal oxygen uptake  
14 ( $\dot{V}O_{2max}$ ) =  $4.4 \pm 0.5$  L/min) provided written, informed consent to participate in this  
15 study. Participants were asked to replicate similar food patterns, refrain from strenuous  
16 exercise and not consume alcohol or caffeine 24 h prior to each exercise trial.

17

### 18 ***Study design***

19 Participants visited the testing facility on seven occasions, each separated by between  
20 48 and 72 h. During visit one, participants were tested for their  $\dot{V}O_{2max}$  and the gas  
21 exchange threshold (GET) using a graded exercise test on a treadmill, as well as being  
22 familiarised to all track-based tests. On visits 2-5, the participants completed fixed-  
23 speed over-ground running trials to exhaustion ( $T_{lim}$ ) at four randomised intensities,  
24 expressed relative to the running speeds attained at GET ( $V_{GET}$ ) and  $\dot{V}O_{2max}$  ( $V_{max}$ ).  
25 Accordingly, these were i)  $\dot{V}O_{2max}$  ( $V_{max}$ ), ii) 110%  $\dot{V}O_{2max}$  (110% $V_{max}$ ), iii)  $\Delta 70\%$  (i.e.  
26 70% of the difference between GET and  $V_{max}$ ) and iv)  $\Delta 85\%$ . All speeds were  
27 determined from treadmill tests to elicit exhaustion within 2 and 15 min (Triska,  
28 Karsten, Nimmerichter, & Tschan, 2017). On visits 6 and 7, the participants performed  
29 all-out 3MT on a 400 m running track to evaluate the test re-test reliability between  
30 days. The CP, CS,  $W'$  and  $D'$  determined from the 3MT on visit 7 were compared to  
31 those determined by the multiple-visit method. Visit 7 was selected as it represented  
32 the most familiarised visit.

1

## 2 **Procedures**

### 3 *Preliminary testing*

4 After a 5-min warm-up at 5 km/h, the participants performed a graded exercise test to  
5 exhaustion on a recently calibrated, motorized treadmill (HP Cosmos Pulsar; HP  
6 Cosmos Sports and Medical, Nussdorf-Traunstein, Germany). The test began at 6  
7 km/h and was conducted at a fixed gradient of 1% to simulate air resistance (Jones &  
8 Doust, 1996). Treadmill speed was increased by 0.5 km/h each minute, until volitional  
9 exhaustion.  $V_{\max}$  was determined as the velocity that corresponded to  $\dot{V}O_{2\max}$ , which  
10 was adjusted ( $V_{\max} = \text{stage speed (km/h)} + \text{time completed (s)} / 60 \times 0.5$ ) when a  
11 stage of the test was not completed. Respiratory gases were collected and measured  
12 breath-by-breath (Jaeger Vyntus CPX, Hoechberg, Germany), with  $\dot{V}O_{2\max}$  determined  
13 as the highest 30-s mean value. The  $\dot{V}O_2$  and  $\dot{V}CO_2$  data were used to plot the GET,  
14 based on a combination of the V-slope method (Beaver, Wasserman, & Whipp, 1986)  
15 and ventilatory equivalents (Caiozzo et al., 1982). The treadmill velocity corresponding  
16 to the GET and  $V_{\max}$  were used to determine the  $\Delta 70\%$  and  $\Delta 85\%$  for subsequent  $T_{\text{lim}}$   
17 trials. Two-thirds of the ramp rate was deducted from GET and  $V_{\max}$  velocities,  
18 accounting for mean  $\dot{V}O_2$  time response during constant work-rate exercise (Whipp,  
19 Torres, Davis, & Wasserman, 1981).

20

### 21 *Over-ground power- and speed-duration relationship determined from multiple visits*

22 For each trial, a 10-Hz GPS device (FieldWiz, ASI, Lausanne, Switzerland) was fitted  
23 between the participant's shoulder blades and secured to the body within a harness  
24 to restrict movement artefacts. The FieldWiz GPS device has provided comparable  
25 (CV = 2.0-5.6%; ICC = > 0.8) and reliable (CV = 0.8-2.2%; ICC = > 0.9) measures of  
26 peak velocity and total distance during linear and multidirectional motion (Willmott,  
27 James, Bliss, Leftwich, & Maxwell, 2019) in relation to a previously validated device  
28 (Varley, Fairweather, & Aughey, 2012). Participants completed a series of four  
29 randomized constant speed tests to  $T_{\text{lim}}$  on the inside lane of a 400 m outdoor synthetic  
30 track at a similar time of day ( $\pm 3$  h). The intensities were all suitable to achieve  $T_{\text{lim}}$   
31 between ~ 2 and 15 min (Jones & Vanhatalo, 2017). The mean temperature and

1 relative humidity were  $12 \pm 6$  °C and  $54 \pm 19$  %, respectively, with wind speeds of  $7 \pm$   
2  $5$  km/h, with  $14$  km/h the highest recorded. The speed of each trial was regulated by  
3 a combination of cones placed at  $10$  m intervals around the inside of the athletics track  
4 and an audio file, which delivered a ‘beep’ sound at a pre-determined frequency. The  
5 participants were asked to control their running speed, such that the audio tone  
6 corresponded to their feet intersecting with each  $10$  m cone. The frequency of the  
7 audio tones was modulated between each trial to match the intended speed of each  
8 participant. The audio file was delivered to the participants through wireless  
9 headphones on a continuous loop. All trials began with a low-cadence walk ( $1.5$  m/s),  
10 and audio tones were increased every  $\sim 20$  s until the prescribed speed was attained.  
11 The participant’s audio track was synchronised to an external device, permitting  
12 monitoring of the participants’ pacing throughout the trials. This process was practiced  
13 during the familiarisation (visit 1). The trial was terminated upon volitional exhaustion  
14 or an inability to maintain the required speed for ten consecutive  $10$  m intervals. In this  
15 instance,  $T_{lim}$  was recorded from the start of the test to the first missed cone. A  
16 handheld stopwatch was used to measure  $T_{lim}$ . Participants were not informed of  
17 elapsed time and no verbal encouragement was provided. If a cone was missed, the  
18 participant was verbally warned and instructed to slowly progress their speed to avoid  
19 sharp accelerations. If the participants were unable to reach the necessary speed in  
20 the subsequent  $10$  cones, the previous criteria were applied. Calculation of the CP or  
21 CS and  $W'$  or  $D'$  was based on linear regression of the work done ( $W$ ) (equation 1) or  
22 distance covered ( $D$ ) (equation 2) vs.  $T_{lim}$  (Monod & Scherrer, 1965) as follows:

23

$$W = CP \times T_{lim} + W' \quad \text{(equation 1)}$$

24

$$D = CS \times T_{lim} + D' \quad \text{(equation 2)}$$

25

26 Where  $W$  is in kJ,  $T_{lim}$  is in s and  $D$  is in m.

27

28 *Over-ground power- and speed-duration relationships determined from the 3MT*

1 Visits 6 and 7 each comprised a 3MT. Both protocols were preceded by a standardised  
2 warm-up, comprising walking, jogging, dynamic stretching and one 10 m sprint.  
3 Participants were instructed to perform a sustained all-out sprint effort in an  
4 anticlockwise direction on either of the two outermost lanes of a six lane 400 m  
5 athletics track. The start line was randomly altered between visits. Strong verbal  
6 encouragement was provided by investigators situated around the perimeter of the  
7 track, although no information on elapsed or remaining time was given to discourage  
8 pacing. The 3MT was terminated once 185 s had elapsed, in order to ensure a  
9 complete 180-s data segment was obtained. The mean speed achieved during the  
10 final 30 s of the test was determined as CS, while the distance (m) > CS ( $D'$ ) was  
11 calculated according to equation 2. Speed data derived from GPS was modelled to  
12 determine mechanical work (J) and over-ground power (W). Critical power (W) was  
13 determined by the mean power output during the last 30 s, while  $W'$  (kJ) was  
14 calculated as work performed (kJ) > CP, according to equation 1.

15

### 16 *Modelling over-ground power*

17 For each outdoor trial (visits 2-7), raw velocity data (10 Hz) were downloaded from the  
18 GPS device and exported to Microsoft Excel (Microsoft Corp., Redmond, USA). From  
19 this, estimations of work and power were made using an energetics model, previously  
20 applied to running-based sports (Cummins, Gray, Shorter, Halaki, & Orr, 2016; Furlan  
21 et al., 2015; Gray et al., 2018), with its underpinning theory validated (Gray et al., 2020;  
22 Zamparo et al., 2019). Drawing upon principles of work-energy theorem, and  
23 established relationships between running speed and the body's kinematics (Gray et  
24 al., 2018; 2020), this model provides estimates of mechanical work done in J and  
25 mechanical power (P) in W on a sample-by-sample basis during over-ground running.  
26 This model partitions total mechanical work ( $W_{\text{total}}$ ) done into external work ( $W_{\text{ext}}$ ) and  
27 internal work ( $W_{\text{int}}$ ), where  $W_{\text{ext}}$  is work done to accelerate the centre of mass (CoM)  
28 with respect to the environment and  $W_{\text{int}}$  is work associated with the acceleration of  
29 body segments with respect to the CoM. Therefore, total mechanical work (J) is given  
30 by:

31

$$W_{\text{tot}} = W_{\text{ext}} + W_{\text{int}} \quad (\text{equation 3})$$

32



1 Additionally, work done can be positive or negative. When the kinetic (KE) and/or  
2 potential energies (PE) of a mass are increased, positive work ( $W_+$ ) is done; when  
3 decreased, negative work ( $W_-$ ) is done. During over-ground running the CoM is also  
4 accelerated in the horizontal ( $W_{hor}$ ) and vertical ( $W_{vert}$ ) planes (Cavagna et al., 1964),  
5 whilst also being subject to air resistance ( $W_{air}$ ) (di Prampero, 1986). Thus, external  
6 work done ( $J \cdot kg^{-1}$ ) is given by:

$$W_{ext} = W_{hor} + W_{vert} + W_{air} \quad (\text{equation 4})$$

8  
9 Using an equation from Minetti (1998), internal work ( $W_{int}$ ) is modelled from velocity,  
10 stride frequency, duty factor (the percentage of the stride cycle in which a single limb  
11 is in the stance phase) and a constant reflecting the inertial properties of the limbs. In  
12 the absence of uneven terrain, varying loads or changes in wind direction and speed,  
13 body mechanics are tightly coupled with forward velocity in running (Gray et al., 2019;  
14 2020). As such, stride frequency and duty factor are readily modelled from GPS  
15 derived running velocity, enabling the subsequent determination of work done to swing  
16 the limbs around the CoM ( $W_{limbs}$ ). Thus, internal work done ( $J \cdot kg^{-1}$ ) is given by:

$$W_{int} = W_{limbs} \quad (\text{equation 5})$$

18  
19 Therefore, starting with knowledge of forward running speed, total work done ( $W_{tot}$  in  
20 J) and P (W) were derived by dividing work done by the sample duration (0.1 s) to  
21 produce a P - time curve. This modelling was applied to raw velocity data for visits 2-  
22 7.

23

## 24 **Statistical analysis**

25 All statistical analyses were performed using Statistical Package for Social Sciences  
26 (SPSS, version 22; SPSS, Inc., IL, USA). Following tests of normality, paired  $t$ -tests  
27 were used to compare the CS,  $D'$ , CP and  $W'$  of the multiple-visit and 3MT, as well as  
28 the test re-test of the 3MT. The absolute error of the method comparison and the  
29 reliability data was evaluated using the coefficient of variation (CV) (Atkinson & Nevill,

1 1998) along with associated 95% confidence intervals. Significant differences were  
 2 identified when  $P < 0.05$ .

3

#### 4 **Results**

##### 5 *Comparison of the 3MT to multi-visit tests*

6 Parameters for each participant are presented for the multiple-visit tests (Table 1) and  
 7 the 3MT (Table 2). There were no systematic differences identified between the  
 8 multiple-visit tests and the 3MT for the CS ( $3.7 \pm 0.2$  vs.  $3.6 \pm 0.4$  m/s,  $P = 0.328$ ) and  
 9  $D'$  ( $145 \pm 38$  vs.  $144 \pm 29$  m,  $P = 0.919$ ), respectively. However, there were differences  
 10 between the multiple-visit tests and 3MT for the CP ( $424 \pm 29$  vs.  $450 \pm 46$  W,  $P =$   
 11  $0.020$ ) and  $W'$  ( $19 \pm 6$  vs.  $25 \pm 8$  kJ,  $P < 0.001$ ), respectively. These values were  
 12 descriptively higher in the 3MT in seven out of the nine participants. The CV ( $\pm 95$  CI)  
 13 for all variables were as follows: CS =  $4.4 \pm 2.9$  %;  $D' = 12.5 \pm 5.1$  %; CP =  $5.1 \pm 1.9$   
 14 %;  $W' = 20.8 \pm 10.3$  %.

15

**Table 1.** Multiple-visit testing parameters derived from the linear distance- and work-time models to characterise the speed- and power-duration relationships. SEE = Standard error of the estimate for  $D'$  (m) and  $W'$  (kJ), respectively.

Partici- pant	$T_{lim}$ (s)				Distance-Time Model				Work-Time Model			
	$\Delta 70$ %	$\Delta 85$ %	$V_{max}$	110% $V_{max}$	Multi- visit CS (m/s)	Multi- visit $D'$ (m)	$r^2$	SEE (m)	Multi- visit CP (W)	Multi- visit $W'$ (kJ)	$r^2$	SEE (kJ)
1	605	341	239	108	3.7	99	1.000	7.9	430	13	1.000	0.4
2	870	606	298	188	4.0	176	0.998	62.8	397	22	0.997	7.5
3	843	600	290	176	3.6	199	0.999	45.5	440	28	1.000	5.4
4	823	620	264	155	3.5	187	0.996	82.8	450	25	0.997	9.8
5	881	670	310	162	4.0	156	0.999	42.7	478	23	0.999	5.8
6	595	412	189	125	3.7	103	0.999	32.9	385	11	0.999	2.8
7	770	457	225	109	3.8	106	0.999	35.8	415	13	0.999	3.3
8	774	443	219	111	3.6	127	0.999	39.2	419	16	0.999	3.8
9	797	495	241	119	3.7	149	1.000	30.9	402	18	1.000	2.8
Mean	773	516	253	139	3.7	145	0.999		424	19	0.999	
SD	105	112	41	31	0.2	38	0.001		29	6	0.001	

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18

1 **Table 2.** Three-minute all-out test (3MT) parameter estimates of the speed- and  
 2 power-duration relationships for trial 1 (3MT 1) and trial 2 (3MT 2).

Participant	Speed-Time Model				Power-Time Model			
	3MT 1 CS (m/s)	3MT 2 CS (m/s)	3MT 1 $D'$ (m)	3MT 2 $D'$ (m)	3MT 1 CP (W)	3MT 2 CP (W)	3MT 1 $W'$ (kJ)	3MT 2 $W'$ (kJ)
1	4.0	3.9	150	125	435	429	28	23
2	3.9	3.8	145	147	455	435	23	23
3	3.6	3.6	195	171	456	474	34	41
4	3.1	3.1	192	200	480	477	29	31
5	3.9	4.2	115	107	500	518	24	23
6	3.0	3.0	128	138	377	361	13	15
7	3.5	3.7	131	123	414	428	24	22
8	3.4	3.6	130	121	452	492	20	17
9	3.7	3.7	171	160	420	432	31	27
Mean	3.6	3.6	151	144	443	450	25	25
SD	0.4	0.4	29	29	37	46	6	8

3

4 *Test re-test reliability of the 3MT*

5 The test re-test reliability of the 3MT demonstrated no systematic differences for CS  
 6 ( $3.6 \pm 0.4$  m/s vs.  $3.6 \pm 0.4$  m/s,  $P = 0.179$ ),  $D'$  ( $151 \pm 29$  vs.  $144 \pm 29$  m,  $P = 0.119$ ),  
 7 CP ( $443 \pm 37$  vs.  $450 \pm 46$  W,  $P = 0.343$ ) and  $W'$  ( $25 \pm 6$  vs.  $25 \pm 8$  kJ,  $P = 0.749$ ). The  
 8 CV ( $\pm 95$  CI) for all variables were as follows: CS =  $2.0 \pm 0.9$  %;  $D' = 5.6 \pm 2.3$  %; CP  
 9 =  $2.6 \pm 1.0$  %;  $W' = 8.1 \pm 3.2$  %.

10

11 Representative traces of speed and modelled power output during the multiple-visit  
 12 tests (Figure 1) and the 3MT (Figure 2) are presented for a single participant.

13

14 \*\*\*\*Insert Figure 1 here\*\*\*\*

15

16 \*\*\*\*Insert Figure 2 here\*\*\*\*

17

18 **Discussion**

19 The current study evaluated the test re-test reliability of the 3MT to characterise both  
 20 the over-ground running speed-duration and, for the first time, modelled power-  
 21 duration relationships. These speed- and power-duration parameters were also  
 22 compared to the traditional multi-visit derivation. There was a consistent performance

1 of the 3MT between repeated visits, with all four parameters producing CV ranging  
2 from 2.0 to 8.1%, and no systematic differences between trials. The CS as derived  
3 from the 3MT compared closely to the multiple-visit testing (4.4% CV), yet  $D'$  had  
4 greater variation (12.5% CV). However, CP and  $W'$  were higher in the 3MT versus the  
5 traditional multiple-visit tests ( $P < 0.05$ ) with a concomitant higher CV (5.1% and  
6 20.8%, respectively) as compared to the speed-based parameters. Collectively, the  
7 results support the reliability of the over-ground 3MT for both power- and speed-  
8 related indices. Whilst the CS and  $D'$  also compare closely to the multiple-visit test,  
9 modelling over-ground power using the 3MT appears to produce larger parameter  
10 estimates of the power-duration relationship.

11

12 The close comparison of CS between multiple-visit testing and the 3MT (4.4% CV) is  
13 consistent with studies comparing laboratory and field-based single-visit methods  
14 comprising three maximal effort runs, with CV ranging between 0.4 to 3.8% (Galbraith,  
15 Hopker, Lelliot, Diddams, & Passfield, 2014; Triska et al., 2017). The  $D'$  error reported  
16 in this study for the multiple-visit testing and the 3MT (12.5% CV) also compares  
17 closely with the literature, with CV reported between 13.0 to 18.7% (Galbraith et al.  
18 2014; Triska et al., 2017).

19

20 Modelled over-ground power parameters demonstrated less agreement between  
21 testing modes, despite being primarily based upon over-ground speed, with CV ranges  
22 of 5.1 to 20.8% vs. 4.4 to 12.5% for power and speed parameters, respectively. This  
23 was likely related to the computational framework of the adopted energetics model  
24 (Gray et al., 2020). During constant speed running, the model returns  $W_{hor}$  values of  
25 zero i.e. when acceleration is zero, no work is done by the CoM in the horizontal plane.  
26 As such, the work estimates produced by the model are attributable to  $W_{vert}$  (~ 55% at  
27 4 m/s) and  $W_{limbs}$  (~ 40% at 4 m/s) (Gray et al., 2020); components that are modelled  
28 from the findings of prior experimental works on CoM motion (Ito, Komi, Sjödin, Bosco,  
29 & Karlsson, 1983; Lee & Farley 1998) and mechanical internal work during locomotion  
30 (Minetti, 1998; Nardello, Ardigò, & Minetti, 2010). However, despite substantial efforts  
31 to pace the participants during the fixed-speed trials, there is inevitable fluctuation in  
32 over-ground speed. The model correctly equates these accelerations to work done in

1 the horizontal plane ( $W_{hor}$ ). That is; minor unavoidable fluctuations in running speed  
2 translate to a heavier weighting in the work/power domain, thus application of the  
3 model might inherently lead to greater variation in estimated work done, even during  
4 'intended' steady-state trials.

5

6 The effects of minor speed fluctuations on the modelled over-ground power are  
7 observable in Figure 1 for a representative participant, where variation in the intended  
8 flat pacing profile leads to increased corresponding power values, relative to the  
9 change in speed. To demonstrate this, applying the over-ground model to this  
10 participant, a minor acceleration of  $0.2 \text{ m/s}^2$  during 0.1-s segment of a steady state  
11 trial, was equivalent to a combined  $W_{vert}$  and  $W_{hor}$  of 26.3 J ( $\sim 50\%$  of  $W_{tot}$ ). Thus, the  
12 multiple components of modelled work result in a relatively greater magnitude of  
13 variation as compared to speed. The magnitude of these values is, perhaps, best  
14 understood by normalising them to their maxima during the 3MT. In the same  
15 participant, their maximal combined  $W_{vert}$  and  $W_{hor}$  across 0.1-s was  $\sim 141 \text{ J}$ , while their  
16 corresponding maximal acceleration was  $8.8 \text{ m/s}^2$ . Our example values therefore  
17 represent 18.6% and 2.3% of the maximal  $W_{vert} + W_{hor}$  and acceleration, respectively,  
18 which highlights the potential for unequal variation in these measures. Interestingly,  
19 as the  $8.8 \text{ m/s}^2$  acceleration also elicited the highest  $W_{vert} + W_{hor}$  value, this highlights  
20 the important point that all elements of the model will contribute to the overall work  
21 done and that during periods of presumed 'steady state' running the instantaneous  
22 work estimations will be more sensitive to speed changes. The cumulative effect of  
23 this across the constant work bouts translates to higher relative change values of work  
24 compared to speed. Therefore, speed and distance might compare well between  
25 methods but power and work might not. Notably, variations in speed are more frequent  
26 during the 3MT, characterised by the rapid acceleration phase, progressive  
27 deceleration phase and the presumed constant-speed period thereafter. The overall  
28 consequence of this is that running bouts with more speed variation will lead to larger  
29 discrepancies between parameters of power, rather than speed, which is consistent  
30 with our findings. As a result, the CP ( $\sim 25 \text{ W}$ ) and  $W'$  ( $\sim 7 \text{ kJ}$ ) are overestimated by  
31 the 3MT, and the 20.8% variation in  $W'$  could lead to a seemingly inaccurate  
32 quantification of this parameter. While estimated work done is accurately captured by  
33 the model, this disturbs the direct assessment of the two testing methods – particularly

1 where steady states are assumed. Thus, this study highlights the potential  
2 incompatibility of physiological assessments when using the speed-time or power-time  
3 relationship. This might be important to potential users if gold standard measures of  
4 CP, and particularly  $W'$ , are necessary.

5

6 The test re-test reliability values of all variables compared closely to laboratory-based  
7 reports, where the 3MT conducted on a cycling ergometer demonstrated CV values of  
8 1.2% and 5.4% and SEE of 6.4 W and 2.7 kJ for CP and  $W'$ , respectively (Vanhatalo,  
9 Doust, & Burnley, 2007; Wright, Bruce-Low, & Jobson, 2017). Furthermore, estimation  
10 of the speed-duration relationship during over-ground running using the 3MT has  
11 previously demonstrated CV values of 3.0% and 5.1% for CS and  $D'$ , respectively (de  
12 Aguiar et al., 2018). Thus, errors measured herein for the CS (2.0% CV) and  $D'$  (5.6%  
13 CV) in the 3MT are consistent with those reported previously. However, for the first  
14 time, the current study extends these findings to over-ground running CP (2.6% CV),  
15 which compared closely to CS (2.0% CV), as measured by the 3MT. In contrast,  $W'$   
16 and  $D'$  error measured at 8.1% and 5.6% CV, respectively, in the 3MT. The poorer  
17 test re-test reliability of  $D'$  and  $W'$  parameters has been reported previously (Gaesser  
18 & Wilson, 1988; Johnson, Sexton, Placek, Murray, & Pettitt, 2011), wherein  $D'$  and  $W'$   
19 consistently produced greater variability in comparison to the CS or CP.

20

21 The greater variation in CP and  $W'$  might be further explained by nuances of the over-  
22 ground energetics model, where variance in total work done can be sensitive to  
23 fluctuations in horizontal speed (i.e. accelerating and decelerating). It is feasible that  
24 slightly poorer reliability of the power-duration model is related to the sensitivity of the  
25 energetics model in estimating work done across stages of the 3MT involving  
26 acceleration and deceleration. This is particularly noteworthy during the initial  
27 acceleration phase, which is demonstrated effectively in Figure 2. Here, the integral of  
28 the power-time relationship above CP during initial acceleration (i.e.  $W'$ ) in this  
29 representative participant is descriptively larger in test 1 compared to test 2. During  
30 acceleration, approximately 25% of the variance in work done is explained by  $W_{hor}$ ,  
31 where large amounts of total work are achieved (peak values of  $\sim 31$  W/kg) (Gray et  
32 al., 2020). Thus, minor alterations in the initial acceleration profile of participants

1 between visits would lead to increased estimations of total work done ( $W'$ ), thereby  
2 affecting the reliability of the test above that demonstrated by  $D'$ .

3

4 The current data provide the first evidence that a field-based 3MT can produce reliable  
5 parameter estimates of the power- and speed-duration relationship. However, to  
6 appropriately evaluate measurement error (reliability), the CV of the derived  
7 parameters should be considered relative to a signal change of practical relevance  
8 (Atkinson & Nevill, 1998). For example, CS can increase by between 6.0% and 8.6 %  
9 in soccer players following four-week (Clark et al., 2013) and six-week (Karsten et al.,  
10 2016) training interventions, respectively. Based on the current study, the reliability of  
11 the test would permit detection of these changes, since the noise (error of 2.0%) is  
12 less than the signal change. Owing to the paucity of current data relating to over-  
13 ground CP and  $W'$ , it is more challenging to understand the acceptability of our  
14 reliability values. However, unpublished data produced from our laboratory indicates  
15 that the measurement error would be sufficiently small to allow detection of changes  
16 in these variables as a result of a field-based training intervention, which are of a  
17 similar magnitude to speed-based metrics.

18

19 There are a number of potential error sources during the current testing procedure,  
20 such as the type of micro-technology used. In the current study, we used a GPS  
21 device, sampling at 10 Hz. Others have used wrist-mounted accelerometers for similar  
22 purposes, without reporting the technical specification or reliability of the device  
23 (Broxterman et al., 2013). Owing to the reported reliability of the current GPS devices  
24 during this type of locomotion (CV = 2%; Wilmott et al., 2019), this technology would  
25 be the more preferable option for measurement of outdoor over-ground speed. It is  
26 also possible that both of these devices do not provide a valid measure of over-ground  
27 speed; however, GPS devices typically underestimate criterion measures of velocity  
28 at higher movement speeds and during directional changes (Duffield, Reid, Baker, &  
29 Spratford, 2010), which is not the case during the fixed-speed trials or the final 30 s of  
30 the 3MT. The variability of GPS devices at higher speeds could, however, explain  
31 some of the increased error between visits for the  $D'$  and  $W'$ . As discussed above, in  
32 this instance, the accumulation of seemingly minor horizontal speed fluctuations will

1 accrue error in the  $W_{hor}$  portion of the over-ground model. Ongoing improvements in  
2 micro-technology and filtering processes will facilitate more robust characterisation of  
3 the speed-duration and, thus, power-duration relationship. Furthermore, variability on  
4 behalf of the participants (i.e. biological error; Hopkins, 2000) is expected during test  
5 re-test study designs, which contributed to the observed testing error. The reliability  
6 values reported herein, therefore, support the conduct of the current study, which  
7 included a familiarisation trial to assist with the participants' understanding of the  
8 necessary all-out effort. Accordingly, we would advise that a familiarisation trial is  
9 performed by potential users of the over-ground running 3MT.

10

### 11 **Practical considerations**

12 There are several assumptions upon which our modelling of over-ground power was  
13 based. The vertical displacement of the CoM, stride frequency and duty factor were  
14 predicted from knowledge of forward velocity. The effects of fatigue (Brueckner et al.,  
15 1991), size (Saibene & Minetti, 2003), running surface (Lejeune, Willems, & Heglund,  
16 1998), running ability (Paradisis et al., 2019) and other contextual factors on these  
17 kinematic variables were unaccounted. Nonetheless, this serves as a first  
18 approximation until direct field-based measurement of these variables is possible.  
19 Additionally, oscillation of the CoM is quantified by changes in potential energy with  
20 movement in the coronal plane assumed to be negligible (Gray et al. 2020). The  
21 mechanical demand of air resistance encountered from headwinds is also not  
22 considered. However, at submaximal speeds (3 m/s) against a 5 m/s headwind the  
23 difference has been shown to be negligible (0.15 W/kg) (Gray et al., 2020). Moreover,  
24 the mechanical demand of swinging the limbs is based on a prediction equation that  
25 assumes four limbs are straight segments with fixed inertial properties across all  
26 running speeds, which does not account for interindividual differences in limb  
27 kinematics (Minetti, 1998). Nonetheless, the prediction equation provides values  
28 within 1 W/kg of gold standard measures (Pavei et al., 2019), thus offering a robust  
29 alternative to direct measurement.

30

31 The current study has important implications for the application of both the over-  
32 ground running energetics model and its coupling with the critical power concept. We



1 have recently argued for the utilisation of the current energetics model to derive  
2 mechanical work done during team sports performance (Gray et al., 2018). This  
3 permits the sports practitioner to monitor external load during low-speed, yet high-  
4 intensity movements, which are typical of field-based training and competition.  
5 However, using modelled over-ground power to characterise the power-duration  
6 relationship enables the practitioner, for the first time, to establish a well-known  
7 threshold of endurance performance (i.e. CP) and continuously monitor the utilisation  
8 and reconstitution of internal energetic indices, such as  $W'$  using non-invasive  
9 methods. This has been previously achieved in cycling to predict performance (Skiba,  
10 Chidnok, Vanhatalo, & Jones, 2012; Townsend, Nichols, Skiba, Racinais, & Périard,  
11 2017) and during intermittent running (Vassallo, Gray, Cummins, Murphy, & Waldron,  
12 2020). The CP and  $W'$  can also be used to profile athletes, prescribe training  
13 intensities, predict performance and monitor responses to training programmes (Jones  
14 et al., 2010; Jones & Vanhatalo, 2017; Vanhatalo, Jones, & Burnley, 2011), which we  
15 encourage team sports practitioners to do by performing 3MT and modelling over-  
16 ground power (Gray et al., 2020; Vassallo et al., 2020). The 3MT produced reliable  
17 results, which would support its use to detect typical changes in the power-duration  
18 relationship; however using the multiple-visit test or use of the speed-based  
19 parameters would be preferable if the higher estimations of CP (~ 25 W) and  $W'$  (~ 7  
20 kJ) are unacceptable. Of course, sports practitioners may also need to consider the  
21 time constraints of their environment when choosing between the 3MT and multiple-  
22 visit tests.

23

## 24 **Conclusion**

25 The results of the current study demonstrate the reliability of the over-ground running  
26 3MT for both power- and speed-related indices. While the 3MT can be used to produce  
27 reliable speed-based parameters, characterisation of the power-duration relationship  
28 will overestimate CP and  $W'$  compared to traditional multiple-visit tests and produce  
29 more variable results. Therefore, we provide evidence that the current over-ground  
30 energetics model can reliably estimate CP and  $W'$  from GPS speed data during the  
31 3MT, which supports its use for athletic training and monitoring purposes. However,  
32 the overestimation of traditional methods means that there will be some unsuitable

1 applications, depending on the importance of this to the user and their tolerance of  
2 error.

3

4 **Disclosure statement**

5 Authors report no potential conflict of interest.

6

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20  
21



1 **Table and figure captions**

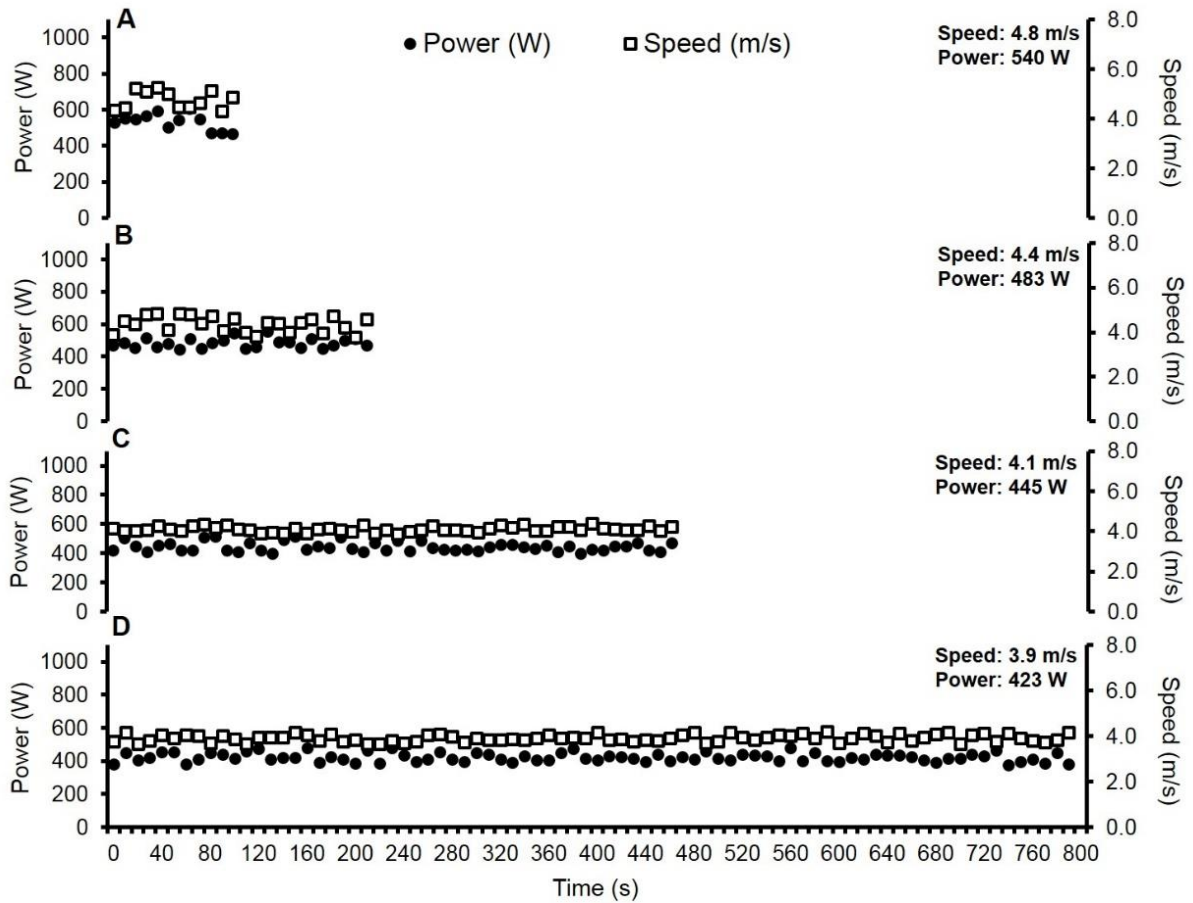
2 Table 1. Multiple-visit testing parameters derived from the linear distance- and work-  
3 time models to characterise the speed- and power-duration relationships. SEE =  
4 Standard error of the estimate for  $D'$  (m) and  $W'$  (kJ), respectively.

5 Table 2. Three-minute all-out test (3MT) parameter estimates of the speed- and  
6 power-duration relationships for trial 1 (3MT 1) and trial 2 (3MT 2).

7 Figure 1. Power output (y-axis) and over-ground speed (yy-axis) during the multi-visit  
8 testing at: 110% $V_{\max}$  (A),  $V_{\max}$  (B),  $\Delta 85\%$  (C),  $\Delta 70\%$  (D) in a representative  
9 participant. Note: Data are presented as 10-s averages; stated speeds and power  
10 outputs are means from that trial.

11 Figure 2. Modelled over-ground power output (A) and raw speed (B) from a 10 Hz  
12 Global Positioning System device during the three-minute all-out test in a  
13 representative participant.

14

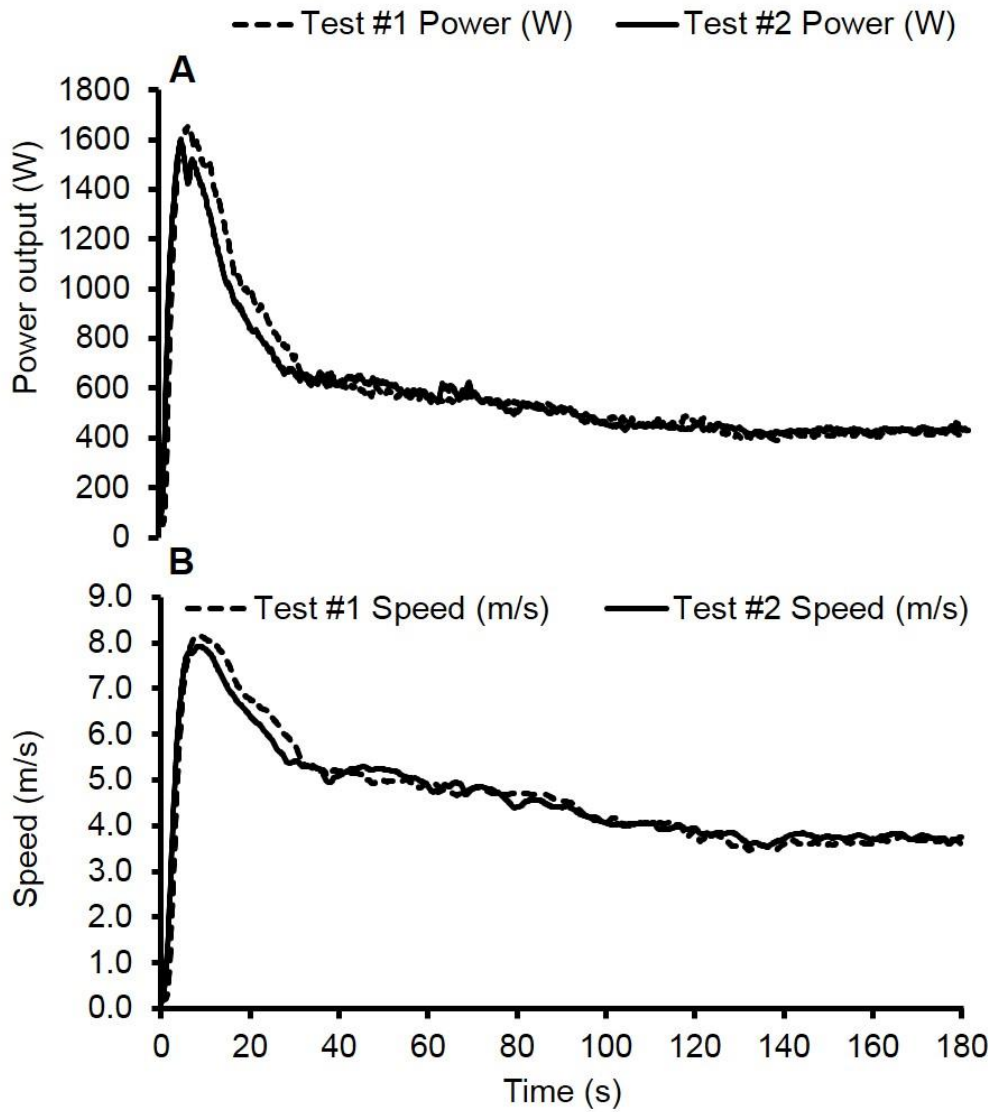


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2 **Figure 1.** Power output (y-axis) and over-ground speed (yy-axis) during the multi-visit  
 3 testing at: 110% $V_{max}$  (A),  $V_{max}$  (B),  $\Delta 85\%$  (C),  $\Delta 70\%$  (D) in a representative participant.  
 4 Note: Data are presented as 10-s averages; stated speeds and power outputs are  
 5 means from that trial.

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1

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 3 Global Positioning System device during the three-minute all-out test in a  
 4 representative participant.