

Unlocking the Application Potential of Forward Osmosis through Integrated/Hybrid Process

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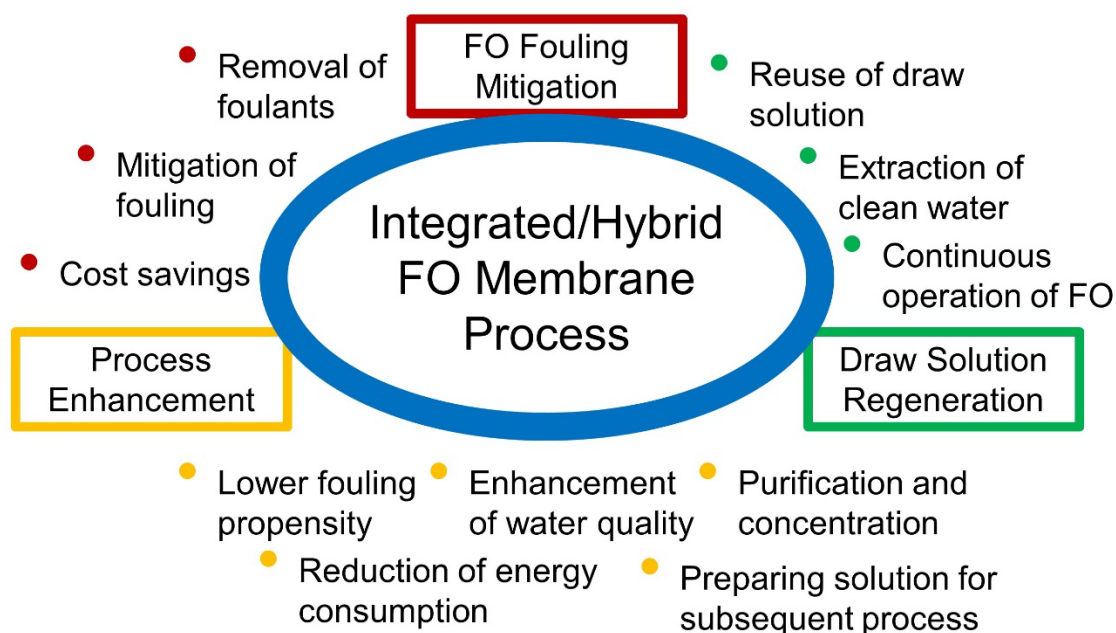
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Graphical Abstract



Abstract

Study of forward osmosis (FO) has been increasing steadily over recent years with applications mainly focusing on desalination and wastewater treatment processes. The working mechanism of FO lies in the natural movement of water between two streams with different osmotic pressure, which makes it useful in concentrating or diluting solutions. FO has rarely been

22 operated as a stand-alone process. Instead, FO processes often appear in a hybrid or integrated
23 form where FO is combined with other treatment technologies to achieve better overall process
24 performance and cost savings. This article aims to provide a comprehensive review on the need
25 for hybridization/integration for FO membrane processes, with emphasis given to process
26 enhancement, draw solution regeneration, and pretreatment for FO fouling mitigation. In
27 general, integrated/hybrid FO processes can reduce the membrane fouling propensity; prepare
28 the solution suitable for subsequent value-added uses and production of renewable energy;
29 lower the costs associated with energy consumption; enhance the quality of treated water; and
30 enable the continuous operation of FO through the regeneration of draw solution. The future
31 potential of FO lies in the success of how it can be hybridized or integrated with other
32 technologies to minimize its own shortcomings, while enhancing the overall performance.

33

34 Keywords: forward osmosis; hybrid and integrated process; desalination; wastewater
35 treatment; draw solution; pretreatment

36

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54

55 **Introduction**

56 In general, a membrane provides a selective barrier which allows the desired substances to pass
57 through while retaining the undesirable substances. This has proved extremely useful in a
58 number of industries. For instance, in the water industries, membranes have been widely
59 employed to produce clean water (for various uses) from different water sources: including
60 surface water, underground water, saline water, and wastewater [1]. In another example, in the
61 food industry, membranes have proven capability in clarifying and concentrating various fruit
62 juices to achieve the desired product quality [2]. In all these cases, the membrane prevents the
63 undesirable compounds, particulates or microorganisms from getting into the final products
64 where the presence of these compounds will limit the usefulness of the treated water or
65 compromise the quality of the final products.

66

67 Membrane technologies are generally recognized have shown improvements over older
68 conventional technologies. For instance, ultrafiltration membranes are capable of removing
69 multiple impurities (turbidity, natural organic matter, and microorganism) presence in water
70 sources that would be harmful to human upon consumption [3]. Not only can ultrafiltration
71 membranes remove multiple impurities in one single unit operation (where several

72 conventional treatment units are required to achieve this), the removal efficiency and
73 performance stability are much better than the conventional treatment processes such as sand
74 filtration. On the other hand, clarification and concentration of juices by membrane processes
75 could maintain heat-sensitive nutritious compounds in the juices [2]. Conventional thermal-
76 based concentration processes normally will destroy nutritious compounds and give the juices
77 undesirable cooked flavors. These issues become minimal with the use of membrane
78 technologies. In short, the advantages of membrane processes over existing conventional
79 processes have contributed to the increasing acceptance of membranes in various water and
80 food industries.

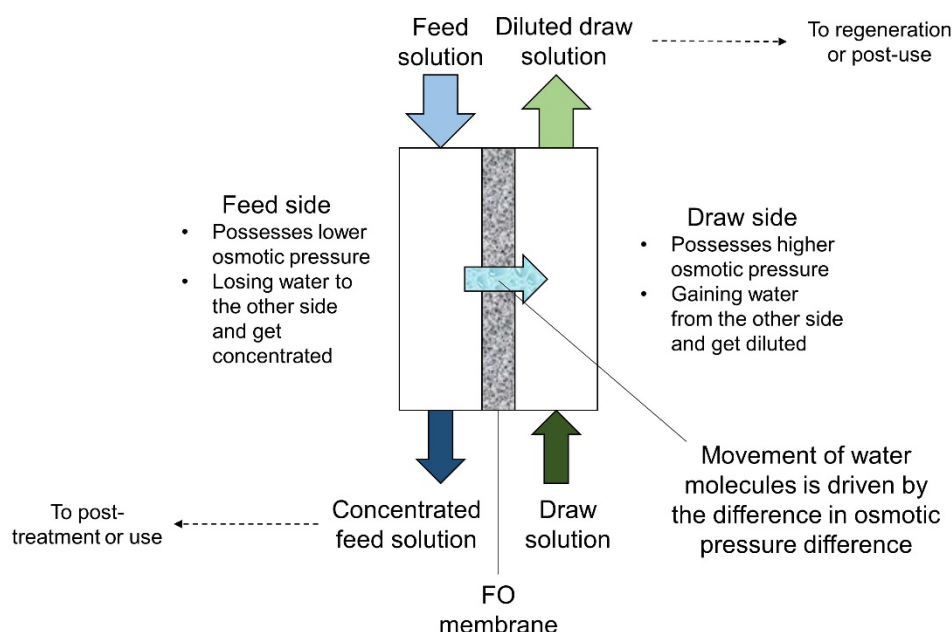
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82 In general, membranes can be categorized into four different classes based on the size ranges
83 for retained particles or solutes: microfiltration (MF), ultrafiltration (UF), nanofiltration (NF),
84 and reverse osmosis (RO) [4]. A substantial number of existing membrane processes are of the
85 pressure-driven type, where the feed solution will be pressurized to drive permeate flow. These
86 membranes have been further innovatively modified to acquire specific properties for other
87 processes. For example, the enhancement of membrane hydrophobicity for membrane
88 distillation (MD) process where the driving force is due to the temperature difference between
89 the feed solution and product [5]. Forward osmosis (FO) is another interesting membrane
90 process, which is driven by the difference in osmotic pressure between two liquid streams, the
91 reversal of reverse osmosis. For FO, the separation capability of the membrane is
92 approximately similar to NF or RO, yet specialized membranes typically have thinner support
93 layers to enhance back diffusion of the solute to reduce concentration polarization [6].

94

95 FO has recently gained considerable attention as an alternative membrane process for various
96 applications. The differences between the FO and the conventional pressure-driven membranes

97 lie in the working mechanism of both operational modes. FO is driven by diffusive flow of
 98 permeate water from a feed stream to a draw solution of higher osmotic potential (Fig. 1). The
 99 working principle is a concentration-dilution concept where the stream losing water will be
 100 concentrated and the stream gaining water will be diluted. This unique property enables FO to
 101 be applied as concentration and dilution processes for many applications, such as juice
 102 concentration, saline water dilution, and wastewater concentration, to name a few [7]. Because
 103 of the lack of applied hydraulic pressure, the membrane fouling propensity has been generally
 104 reported to be lower compared to pressure-driven membranes [8]. However, the
 105 commercialization of FO process has been hindered by several challenges.



106

107 **Fig. 1.** Working mechanism of FO process.

108

109 The first issue associated with FO process is the lack of membranes with suitably high flux and
 110 retention. The flux is linked to production capacity, while high retention is necessary to prevent
 111 undesirable compounds crossing into other streams. Thus far, the existing advanced FO
 112 membranes (mixed matrix, biomimetic, and thin-film composite) still suffer from low water
 113 flux and imperfect retention of impurities (compounds in feed solution and ionic salts in draw

114 solution) [9]. The second challenge relates to the need of draw solution in order to operate the
115 FO process. Unless the draw solution can be obtained easily (such as industrial brine,
116 concentrated fertilizer, and seawater) or the regeneration of draw solution is unnecessary, the
117 use and regeneration of synthetic draw solution requires an additional unit operation [10]. This
118 incurs additional cost for the FO process. Though FO has been frequently known as a low
119 energy process, this claim is only valid if regeneration of draw solution is not required.
120 Increasing treatment cost will be a major hindrance for the commercialization and acceptance
121 of FO process in the industry. Lastly, FO is rarely operated individually, mainly due to the need
122 for an additional process for draw solution regeneration and clean water extraction from draw
123 solution.

124

125 The research on the FO process has not diminished despite the challenges encountered by this
126 technology, with the number of reported articles hitting more than 250 in 2018 [11]. The main
127 category of studies that have been driving the FO research was membrane synthesis and FO
128 application. Considering that a large portion of the reported studies were about application and
129 performance studies, one might question in what way that the FO process can be utilized and
130 be beneficial to the industry, giving the fact that FO could not be operated individually to
131 achieve the application aims. A quick glimpse into the research articles revealed that most of
132 the application and performance evaluation studies of FO have been conducted in integrated or
133 hybrid process form, where the FO process is combined with other technologies to achieve a
134 certain application targets.

135

136 **Definition of Integrated and Hybrid FO Membrane Process**

137 A hybrid process is defined as a single system that possesses multiple functions by combining
138 the individual treatment processes while the integrated process is generally categorized as the

139 combination of different processes with different functions into a single treatment train [1,12].
140 Though FO process reportedly shows prospective potential in various niche applications, it is
141 generally accepted by the scientific community that a standalone FO process appears to be less
142 attractive and competitive. This shortcoming lies in the operation concept of FO process where
143 it is more to concentration-dilution process and the need of draw solution in most of the
144 applications. To advance the FO process and to realize its prospective application in various
145 industries, innovative design of hybridization and integration involving FO process and other
146 technologies have been actively proposed and sought by the research community. This review
147 paper discussed the studies of the FO process, how it is innovatively hybridized or integrated
148 with other technologies to achieve particular aims and to resolve certain challenges associated
149 with FO or other processes. The hybrid/integrated FO process will be discussed based on three
150 main purposes of having hybridization/integration: process enhancement, draw solution
151 regeneration and fouling mitigation.

152

153 **Process enhancement**

154 FO process can be integrated/hybridized with other technologies to enhance the capability of
155 the latter process or to improve the FO performance. The improvement can be in the forms of
156 process efficiency, cost, or minimization of operational problems. In this section, the
157 integrated/hybrid FO process will be discussed based on the main application categories:
158 desalination, wastewater treatment and reclamation, bioproducts and food industry, and energy
159 generation and resources recovery.

160

161 Desalination

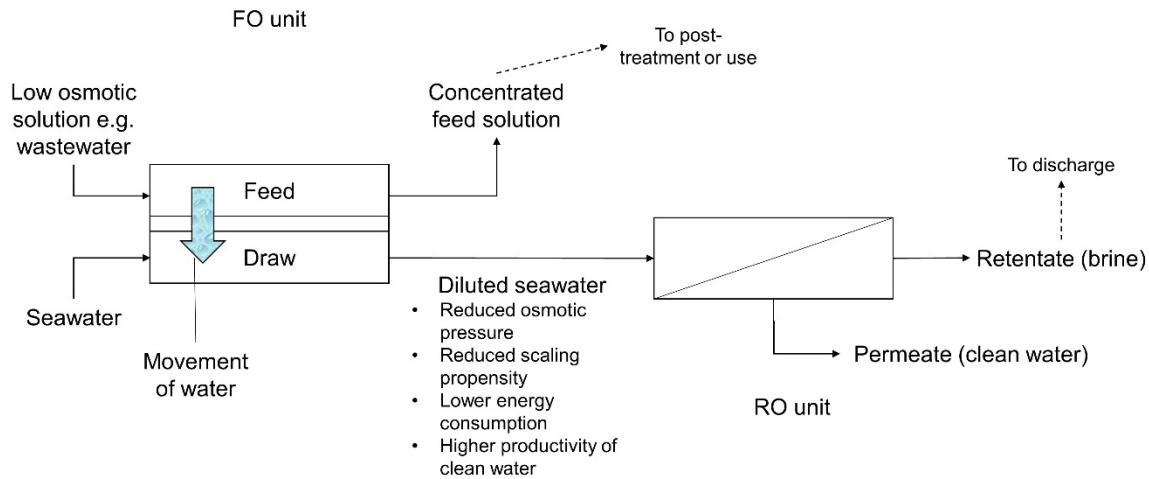
162 Desalination is one of the major technologies that is a potential solution to water scarcity. A
163 number of thermal- and non-thermal-based desalination technologies have been developed

164 worldwide, with the former technology mainly applied in Middle East countries while the latter
165 (mostly RO membrane desalination) in the rest of the world [13]. Desalination technologies
166 successfully supply clean water to populations, but its operation is still burdened with
167 considerably high energy consumption that drives up the water cost. This particular issue can
168 be attributed to the high salt contents of seawater, which requires more pumping energy to
169 extract the clean water from the seawater as compared to conventional surface waters. In view
170 of this, FO process has been innovatively integrated with desalination technologies to improve
171 the overall performance and cost-practicality of seawater desalination [9]. The main function
172 of the FO process is to provide a platform that enables the dilution of feed to the desalination
173 plant, which subsequently offers the opportunity to lower energy consumption or scaling issue.

174

175 Owing to its concentration-dilution working principle, the FO process has been proposed to be
176 integrated prior to seawater reverse osmosis desalination system. The seawater will be fed to
177 the FO process as draw solution and it will be diluted by pulling water from the feed solution
178 that possesses lower osmotic pressure (e.g. low salinity wastewater) [14,15]. The osmotic
179 pressure of the diluted seawater will be lowered after passing through the FO process as shown
180 in Fig. 2. The dilution of seawater has a positive impact on the RO desalination process, as the
181 scaling propensity (salts precipitation formation) will be reduced and the lower osmotic
182 pressure can be translated to lower energy consumption (either through lower operating
183 pressure or higher flux productivity). For instance, Yangali-Quintanilla et al. (2011) showed
184 that by using secondary wastewater as feed solution, the FO process can reduce the total
185 dissolved solids (TDS) of Red Sea seawater (draw solution) from 40.5 g/L down to 15 g/L [14].
186 The huge reduction in TDS has halved the energy consumption of subsequent low-pressure RO
187 desalination process, making it possible to achieve energy consumption of 1.5 kWh/m³ instead
188 of 2.5-4 kWh/m³ for standalone RO desalination process. However, this finding is only

189 practical if the minimum average FO flux is at $5.5 \text{ L/m}^2\cdot\text{h}$ (the average FO flux in this study
 190 was below $3 \text{ L/m}^2\cdot\text{h}$). Furthermore, this concept is only practical if the wastewater treatment
 191 plant and desalination plant are located close to each other, else the costs associated with
 192 transporting and handling the wastewater might be a burden for the operators [16].



193

194 **Fig. 2.** Integrated FO-RO process for seawater desalination.

195

196 A pilot plant consists of integrated FO-RO utilizing wastewater from coal-fired power plant as
 197 feed solution to dilute the seawater (draw solution) has been conducted by Choi et al. (2017)
 198 for 5 months of operation period [17]. The energy consumption analysis revealed that the
 199 energy consumption for desalinating the diluted seawater by FO was 23.3% less than a typical
 200 seawater desalination by RO, with specific energy consumption (SEC) for the integrated FO-
 201 RO at $2.85 \pm 0.05 \text{ kWh/m}^3$ and seawater RO at $3.34 \pm 0.05 \text{ kWh/m}^3$. This led the an
 202 approximately 15% lower total energy consumption.

203

204 The feasibility of integrated FO-RO process for desalination has also been evaluated via
 205 techno-economic evaluation study [18]. Wan et al. (2018) investigated the technical and
 206 economic feasibilities of different combination of integrated RO process, including the
 207 arrangement of FO for post-dilution process to dilute and recycle the RO brine and FO as pre-

208 dilution process to reduce the RO operating pressure [18]. It was reported that the pre-dilution
209 of FO could reduce the operating pressure of RO (25% recovery) from 42 bar to 31 bar,
210 resulting in a saving up to \$905,000/yr. For 50% recovery, the operating expenditure of RO
211 can be further reduced and achieve highest saving up to \$2081,000/yr when the FO process is
212 integrated with existing RO plant. On another note, the construction of new integrated FO-RO
213 seawater desalination plant can effectively reduce both operating and capital expenditures, with
214 a much higher savings up to \$4390,000/yr. The savings were mostly attributed to the lower RO
215 operating pressure.

216

217 Indeed, the economic evaluation done on a similar integrated FO-RO desalination process
218 could only be beneficial if substantial energy and operational costs savings are achieved [19].
219 Moreover, the threshold flux for FO should be at least 30 L/m².h to guarantee FO economic
220 sustainability where none of the existing FO membrane has recorded such a high flux value.
221 One of the plausible ways to achieve higher FO flux is to apply pressure at the feed side of the
222 FO process to increase the permeation of water from feed to draw solutions. This operation is
223 known as pressure-assisted forward osmosis (PAFO) where it could increase the overall water
224 recovery and reduce the reverse salt flux of FO process. However, the mechanical strength of
225 the FO membrane and the associated additional energy consumption might be the major
226 challenges for the feasibility of this operation mode. The energy penalty posed by the pressure-
227 assisted operational mode could potentially be compensated by enhanced permeate throughput
228 and reduced membrane area [20]. The economic potential of integrated PAFO-RO has been
229 proven higher than integrated FO-RO process, though the plausibility of implementing PAFO
230 to existing RO plants still remain uncertain due to the additional capital expenses associated
231 with PAFO [21].

232

233 In another study, numerical modelling of integrated FO-RO desalination process has shown
234 that the integrated process performed better than the stand-alone RO process in terms of SEC
235 and recovery rate. At an operating pressure of 30 bar for RO process, the SEC of the integrated
236 system was 2.68 kWh/m³ lower than the stand-alone RO process. In addition, the RO recovery
237 rate of the integrated process was 28% higher than the stand-alone RO process [15]. These
238 values were acquired after considering the energy consumption associated with the FO process.
239 Such positive outcomes could be obtained as the typical energy-intensive consumption part
240 (regeneration of draw solution) was not required since the diluted seawater was used as the
241 feed for RO process. Similar positive costing analysis has also been reported by Linares et al.
242 (2016) where compared to standalone seawater RO desalination process, the integrated FO-
243 low pressure RO process recorded 56% lower operational costs (due to savings in energy
244 consumption and fouling control) and 16% lower total water cost per cubic meter of water
245 produced [22]. Pilot-tested of real desalination plant has also been constructed and it was
246 reported that compared to conventional seawater RO desalination system, the integrated FO
247 process (draw solution and regeneration technique were kept confidential by the company)
248 could be operated at about 60% of the energy consumption of the competing seawater RO
249 facility [23].

250

251 Similar integration configuration has also been tested for the thermal-based desalination
252 process. FO process was integrated with multi-stage flashing (MSF) desalination where the
253 brine reject from real MSF desalination plant and seawater were used as the draw and feed
254 solutions, respectively [24]. It has to be noted that the brine reject from MSF is normally
255 recycled back to the evaporator, meaning that the system is vulnerable to high scaling
256 propensity (formation of salt precipitates) due to the accumulation of divalent salts such as
257 calcium, magnesium and sulfate. To prevent scale deposition in the MSF plant, the brine reject

258 was diluted through FO process since its osmotic pressure was higher than seawater feed
259 solution. An experimental study with real samples has indicated that 3-9% of brine reject
260 dilution was achievable, depending on the operating temperature. The findings supported the
261 theoretical simulation studies where FO can be used as a medium to dilute the brine reject [25].
262 Dilution of brine reject will potentially lower down the scaling deposition propensity in the
263 MSF plant and increase the overall recovery rate. Further pilot plant test is required to prove
264 the practicality of the integrated FO-MSF desalination process and to verify the increment of
265 recovery rate contributed by FO process.

266

267 The FO process has also been proposed to be integrated with processes such as nanofiltration
268 and electrodialysis for seawater and brackish water desalination purposes [26–29]. Both
269 experimental and simulation modelling studies have shown that the integration of FO managed
270 to dilute the feed water for subsequent nanofiltration and electrodialysis desalination. These
271 integrated processes can produce permeate water meeting drinking water standards. For
272 instance, the optimization simulation done by Bitaw et al. (2016) showed that FO could be
273 integrated prior the electrodialysis process to provide good feed water for more efficient
274 electrodialysis desalination process [28]. Since the FO process was utilizing draw solution in
275 the operation, it provided an access to a wide range of ionic species with higher mobility than
276 NaCl and other trace ions in seawater. The use of FO draw solution as feed for electrodialysis
277 resulted in lower electrical resistance for electrodialysis operation and eliminated the risk of
278 membrane fouling issue. Economic feasibility analysis revealed that the use of ammonium
279 chloride as draw solution for FO process could give the lowest total unit product water cost
280 with 0.51 USD/m³ for the integrated FO-electrodialysis-RO process, which was much lower
281 than existing seawater RO desalination system. However, the practicality and up-scaling of

282 these processes remain uncertain as only limited literature, especially on costing aspects, is
283 available.

284

285 Besides being integrated as a pretreatment prior to other main desalination technologies, FO
286 has also been proposed to be integrated after the desalination technologies to achieve zero-
287 liquid discharge treatment system [30]. Utilizing a thermolytic draw solution, FO can further
288 concentrate the brine discharged from seawater RO desalination plant before being sent to a
289 crystallizer. The crystallizer will precipitate the salts, while the diluted draw solution will be
290 regenerated using low-temperature distillation processes. This helped to close the loop of a
291 desalination process and is especially suitable for inland brackish desalination plants where the
292 discharge of brine is unfavorable due to its disruptive effects on the local environment.

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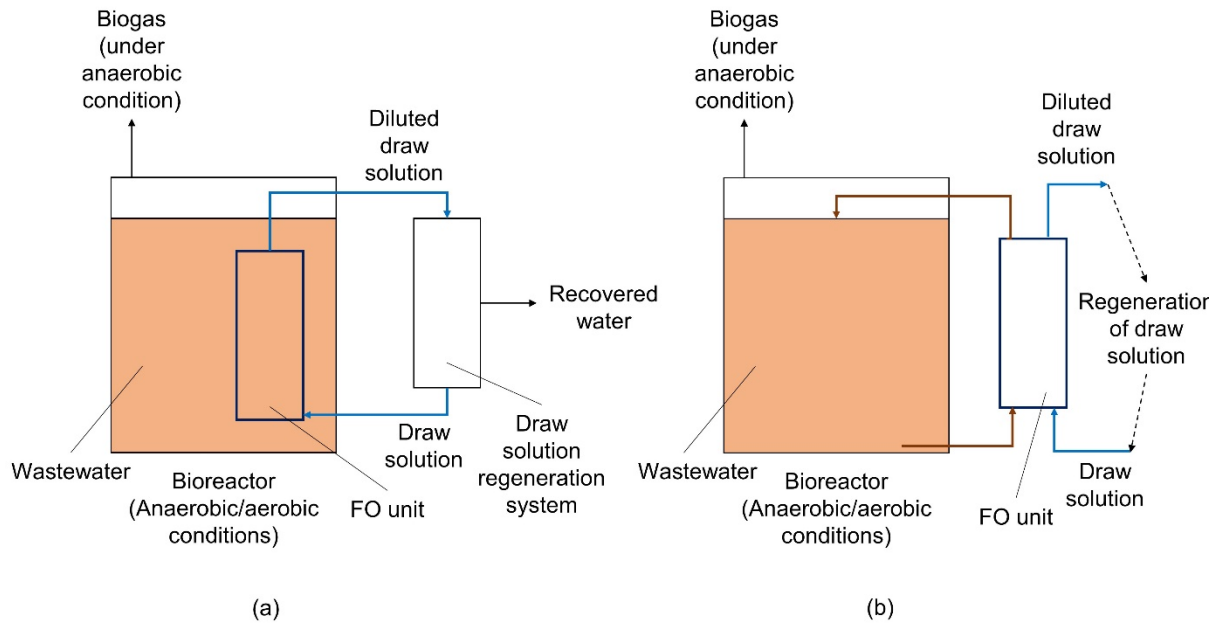
294 Wastewater Treatment and Reclamation

295 Wastewater is defined as any water where the quality has been affected by human use (from
296 sources such as domestic, industrial, commercial, and agricultural activities), from surface
297 runoff (stormwater), and sewer inflow or sewer infiltration [31]. The characteristics and
298 constituents of wastewater vary depending on the sources, which may be harmful to the
299 environment and living organism if left untreated and disposed to the waterways. Generally,
300 the treatment of wastewater can be divided into three broad categories: physical, biological,
301 and chemical; according to the main working mechanism [12]. Among these technologies,
302 membrane has emerged as one of the most promising physical treatment processes and has a
303 proven track record in various wastewater treatment systems [32]. Membrane processes are not
304 only more effective than conventional processes but its versatility lies in the capability to be
305 integrated or hybridized with other treatment technologies, giving the whole treatment system
306 greater capability in removing multiple undesired pollutants [33]. Similar to conventional

307 pressurized-membrane processes, FO has also found its potential in wastewater treatment
308 processes, where it can be used for concentration: reducing the amount of wastewater or
309 extracting clean water from the wastewater by using draw solution. Integrated/hybrid FO
310 process will be discussed based on the following categories: hybrid FO process (combining
311 several processes into one treatment unit) and FO process integrated with other technologies
312 for treatment or clean water extraction (regeneration of draw solution) purposes.

313

314 Membrane bioreactor (MBR) is a hybrid membrane process that combines microfiltration or
315 ultrafiltration with a biological wastewater treatment process, such as activated sludge. MBR
316 is now being widely used for municipal and industrial wastewater treatment for treatment and
317 non-potable reuse applications. The better quality of treated water and consistent treatment
318 efficiency in a smaller footprint as compared to conventional treatment processes are some of
319 the main reasons for the wide acceptance of this hybrid membrane process [34]. However, the
320 treated water may still contain low molecular weight constituents, such as trace organic
321 compounds (TrOCs), ions, and viruses that are hardly rejected by microfiltration or
322 ultrafiltration membranes [35]. To enhance the quality of the treated water without exerting
323 additional cost (energy) or exacerbating the membrane fouling propensity, FO membrane has
324 been proposed as a replacement for microfiltration and ultrafiltration in MBR. The new hybrid
325 process – osmotic membrane bioreactor (OMBR) can produce treated water with a lower
326 concentration of low molecular weight impurities, since FO membrane has better retention
327 capability compared to MF or UF [36]. OMBR can be operated in two modes – with FO
328 membrane placed inside or outside the bioreactor, as shown in Fig. 3 [37]. The draw solution
329 will extract water from the bioreactor fed with wastewater. An additional process will have to
330 be applied for water reclamation and regeneration of draw solution.



331

332 **Fig. 3.** Schematic diagram of OMBR (a) FO submerged in the bioreactor; (b) side-stream
 333 drawn out for FO unit (adapted from [37]).

334

335 The performance of OMBR has been actively investigated, with promising results indicating
 336 the potential of OMBR for various wastewater sources [38]. Improvement in terms of rejection
 337 of TrOCs, nutrients, and organic substances has been achieved with the incorporation of FO in
 338 the conventional MBR process [36,38]. In addition, OMBR has also been employed to increase
 339 the solid concentration for anaerobic digestion [39]. The dewatering capability of FO enabled
 340 water to be continuously drawn out from the bioreactor and led to the concentration of solid
 341 contents. As the total solids content in the bioreactor was gradually increased, the associated
 342 methane (biogas) production and organic degradation have also been enhanced. This implies
 343 the potential of the FO process in enhancing the performance of anaerobic digestion (for biogas
 344 production) while operating in a smaller footprint and at the same time supporting the effort
 345 for sustainable wastewater management [40]. Also, the concentration of anaerobically treated
 346 wastewater by FO process could lead to the enrichment of nutrients (especially phosphorus) in
 347 the wastewater and subsequently to be recovered as struvite crystal [41]. However, the high

348 retention of pollutants by the FO membrane indicates that the pollutants will have a high
349 tendency to be accumulated and concentrated in the bioreactor. Reverse diffusion of draw
350 solution would also contaminate the bioreactor with draw solutes. Past studies have
351 demonstrated that the accumulation of pollutants or the presence of draw solutes in the
352 bioreactor will affect the microbial activity (biodegradation of pollutants), resulting in lower
353 treatment efficiency (e.g. nutrients removal and organic matter degradation) of the hybrid
354 process [38,42]. The build-up of salinity in the bioreactor will also reduce the FO membrane
355 flux since the osmotic pressure difference between the feed and draw solutions has been
356 lessened.

357

358 To overcome these issues, the OMBR process has been integrated with either MF or UF
359 membranes to continuously draw out a portion of water from the bioreactor [38,43–46]. For
360 instance, OMBR integrated with MF (MF-OMBR) could achieve a long-term continuous
361 operation with high methane (biogas) production from the anaerobic bioreactor due to the
362 consistent salt level [45]. The water drawn out by MF membrane prevented salt accumulation
363 in the reactor and can be further treated or processed to recover the phosphorus nutrient. The
364 additional benefit was that the FO membrane flux could be maintained since the osmotic
365 pressure difference between the wastewater and draw solution has remained constant. A long-
366 term pilot scale of UF-OMBR process has further confirmed the benefits of integrating UF
367 process in the typical OMBR system [47]. The integrated system managed to operate for more
368 than 120 days while consistently producing high quality RO permeate (draw solution
369 regeneration) from domestic wastewater. The FO membrane recorded a stable flux of 4.8
370 L/m².h with minimal flux decline throughout the whole operation period. Though the proposed
371 approach seems to resolve part of the issues associated with OMBR, the issues of effluent

372 quality from UF or MF membranes and the FO membrane fouling needs to be taken into
373 consideration before the integrated OMBR process can be applied commercially.

374

375 Since the FO membrane is exposed to wastewater laden with an abundance of suspended solids
376 and impurities, it is vulnerable to organic fouling of the membrane surface. In order to eliminate
377 the membrane fouling issues, Qiu et al. (2016) replaced the MF membrane with biofilm (BF-
378 OMBR) for the treatment of municipal wastewater [48]. The side-stream effluent from the
379 bioreactor was drawn out without any filtration process and hence recorded slightly lower
380 removal of organic matter and nitrogen. Despite the comparatively lower removal of impurities,
381 the incorporation of fixed-bed biofilm mitigated the FO membrane fouling by 25-55% as
382 compared to MF-OMBR. The improvement of FO performance could be attributed to the
383 washing-out of suspended growth and dispersed cells in the reactor (due to the absence of MF
384 membrane), leaving behind the attached growth of the biofilm. Subsequently, the deposition of
385 impurities on the FO membrane has also been minimized in the case of BF-OMBR.
386 Modification of OMBR has also been done by Juntawang et al. (2019) where the bacteria in
387 the reactor was grown and entrapped within a polymeric matrix [49]. The entrapped bacteria
388 in the anaerobic reactor was more resistance to the effect of reverse salt flux as compared to
389 the suspended cells found in a typical OMBR. The salt stress will lead to cell dehydration and
390 the release of extracellular polymeric substances and soluble microbial products, two
391 substances that are normally associated with membrane fouling in MBR [50,51]. This might
392 explain why the entrapped cells OMBR showed a lower FO membrane fouling propensity,
393 since the bacteria were more resistant to salt stress leading to lower release of extracellular
394 polymeric substances and soluble microbial products (13-68%).

395

396 FO can also be integrated with other technologies such as coagulation, microfiltration,
397 adsorption, ultrafiltration, electrocoagulation, multimedia filtration, and electrochemical
398 processes [52–58]. Each integrated process serves a different purpose, be it improving the
399 conditions of the feed water for FO process or increasing the pollutant removal efficiency of
400 the whole treatment system. For instance, the incorporation of electrocoagulation has managed
401 to remove the total organic carbon and total suspended solids up to 78% and 96%, respectively,
402 the two main pollutants present in produced water that could severely foul the FO membrane
403 [57,59]. The installation of MF membrane prior to FO process has also succeeded in removing
404 the total organic carbon (~52%) and turbidity (~98.5%) in fracking wastewater [58]. In these
405 cases, FO membrane performance was stable with minimal fouling due to the reduction of
406 impurities in the feed solutions. Consequently, clean water can be extracted while draw solution
407 can be regenerated through the downstream MD process.

408

409 A considerable number of studies have been made of the FO process integrated with membrane
410 technologies (especially MD and RO) to regenerate the draw solution and to recover the
411 extracted clean water [60–69]. In this integrated process, FO was used to extract water from
412 various wastewater sources, such as sewage, produced water, human urine, effluent from the
413 leather industry, and coal mine wastewater, to name a few. The volume of the wastewater
414 would be reduced due to concentration process by FO, which would be beneficial in terms of
415 space management and handling cost. On the other hand, the diluted draw solution needs to be
416 regenerated or else the FO process will fail to operate (low osmotic pressure difference will
417 lead to low water flux). Hence, the integration of FO with other technologies for draw solution
418 regeneration is vital to ensure the continuous operation of FO process and extraction of clean
419 water.

420

421 In another case, the regeneration of draw solution was eliminated with the use of fertilizer as
422 the draw solution. Chekli et al. (2017) reported that the FO process could be used to concentrate
423 the synthetic wastewater with fertilizer as the draw solution, though the FO process has to be
424 integrated with pressure assisted osmosis (similar operation as FO process but the feed stream
425 was subjected to 2 bar of pressure) to further dilute the fertilizer draw solution to the level
426 suitable for hydroponic application [70]. Preliminary assessment of energy and cost analysis
427 showed that by combining both the FO process and pressure assisted osmosis could lead to
428 reduction in membrane replacement cost, albeit the overall operating cost was slightly higher
429 (due to the additional energy requirement for pressure assisted osmosis process) than
430 standalone process. This indicated the trade-off between the different aspects when designing
431 the integrated process for optimal energy and expenditure costs.

432

433 Bioproducts and Food Industry

434 Concentration technology is an important process in various industries to obtain products with
435 desirable quality and to save costs associated with shelf life, storage, and transportation. For
436 instance, fruit juices are generally concentrated from raw juices to increase their shelf life and
437 to save space for storage and cost for transportation [71–73]. The typical technologies
438 employed for fruit juices concentration are multi-stage vacuum evaporation, freezing technique,
439 and membrane (NF & RO) processes. These processes possess some drawbacks, such as being
440 energy-intensive, have negative impacts on juice quality, and high membrane fouling issues
441 [74]. Currently, FO has been proposed as an alternative technology for fruit juice concentration,
442 aligns with its working principles [75]. Though numerous studies have demonstrated the
443 capability of FO in concentrating the fruit juices to a desirable concentration, studies on
444 integrated FO process for this application have been rare. An integrated FO process reported
445 in the literature was the integration of FO with MD where the latter process served to regenerate

446 the draw solution and to ensure continuous operation of FO process [74]. The integrated FO-
447 MD process managed to increase the total soluble solid of apple juice from 10.6°Brix to
448 45.1°Brix, which was twice the value achieved by an RO concentration process. The nutrition
449 loss was minimal and the presence of draw solute - potassium sorbate (food preservative) in
450 the concentrated juice was far below the allowed level in food industry. This study showed that
451 the integrated FO process may have practical application potentials in the juices concentration
452 process.

453

454 In the production of Greek-Style Yogurt, a considerable amount of Greek yoghurt Acid Whey
455 (GAW) is also produced. GAW can be disposed as wastewater after proper treatment, but also
456 contains some milk solids (proteins, lactose, and minerals), which can be recovered and used
457 as ingredients in value-added products such as beverages, sauces, snacks or baked goods [76].
458 However, the concentration of these useful substances was low (approximately 6%), making it
459 difficult to be processed, stored, or transported. In view of this, non-thermal concentration
460 processes such as RO have been utilized to concentrate the solution by removing water.
461 Unfortunately, the application of RO process revealed drawbacks such as high membrane
462 fouling and limited attainable concentration due to concentration polarization. In this context,
463 Menchik et al. (2019) have integrated RO and FO processes to concentrate GAW [76]. The
464 GAW was first concentrated by RO from initial total soluble solid of 6.6°Brix to 19.6°Brix
465 where the pre-concentrated GAW was then further concentrated by FO process to acquire a
466 total soluble solid of 40.2°Brix. The role of FO was to further concentrate the GAW as the
467 limitation of concentration has been achieved for RO and no further concentration is possible
468 due to high concentration polarization and membrane fouling. With the integrated RO-FO
469 process, the GAW attained the concentration levels comparable or higher than thermal

470 evaporation. More encouraging was that the integrated membrane process did not cause any
471 thermal damage on the GAW concentrate.

472

473 In another similar application, the costing analysis of water recovery and whey powder
474 production from cheese whey waste using integrated FO process has also been conducted. This
475 is especially important as the FO process has been argued to increase the costs considerably
476 due to the need for draw solution regeneration. By using process modeling and cost estimation
477 software program, Aydiner et al. (2014) reported that the integrated FO-RO process managed
478 to achieve the highest water recovery (from the regeneration of draw solution through RO
479 system) at 77% and possess payback period at par with the conventional UF-RO process for
480 the concentration of whey and water recovery [77]. Such positive techno-economic finding
481 could be attributed to the better whey concentration efficiency by FO as compared to UF, which
482 subsequently led to higher whey powder production rate (translated to higher revenue from
483 whey powder sale) in the downstream process. The techno-economic evaluation was proceeded
484 by replacing the RO with MD for the regeneration of draw solution. The payback time of the
485 investment for integrated FO-MD process in dairy wastewater treatment was less than 1 year
486 due to annual revenues of about 3.4 million \$ from water recovery and whey powder selling
487 [78]. This further strengthened the role of integrated FO process in promoting sustainable waste
488 management with good economic benefits.

489

490 Integrated FO process has also been applied for protein concentration. Proteins (and other
491 biopolymers) have a wide range of commercial applications in nutraceutical, medical, and
492 pharmaceutical markets [79]. Since most proteins are labile and sensitive to heat, non-thermal
493 separation and purification are required for their concentration. Ling et al. (2011) proposed a
494 dual-stage FO system for protein enrichment using nanoparticles capped with polyacrylic acid

495 as the draw solution [80]. The protein solution was concentrated in the first FO stage while the
496 regeneration of draw solution was conducted in the second FO stage with synthetic RO brine
497 to regenerate the nanoparticle draw solution. It was reported that the protein molecules
498 remained intact and stable during the enrichment process which could be attributed to the
499 minimal reverse salt flux. The success of this indicates that integrated FO process can be used
500 for the application of other pharmaceutical and bio-molecule concentration and purification
501 processes.

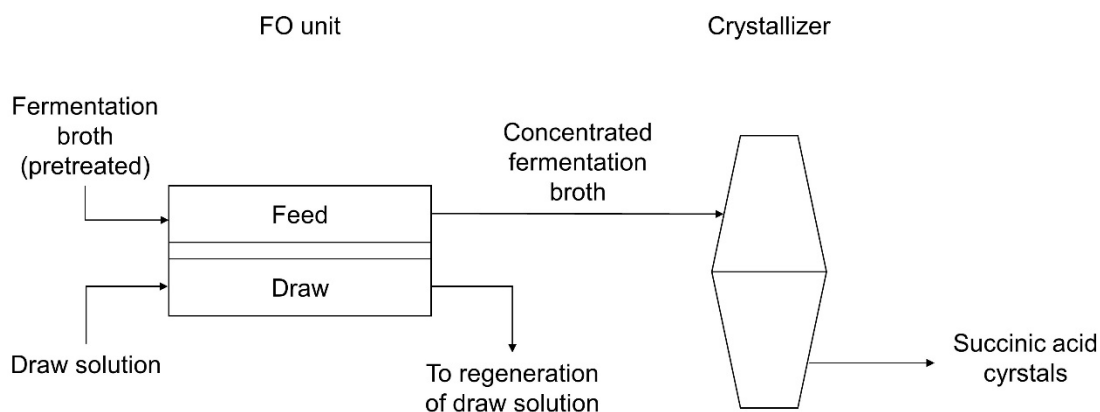
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503 Bioenergy has emerged as a source of renewable energy. It can be produced from easily
504 available waste materials, such as the liquid fraction from hydrothermal pretreatment of rice
505 straw that contains sugar, which is the nutrient source for the production of bioethanol through
506 fermentation process [81]. However, the concentration of sugar in the liquid fraction was too
507 low for efficient bioethanol production. The production efficiency was further reduced with the
508 presence of fermentation inhibitors. To facilitate more efficient production of bioethanol, FO
509 has been adopted to concentrate the liquid fraction before the fermentation process [82]. FO
510 was used to increase the sugar concentration in the liquid fraction (feed solution) while at the
511 same time maintaining the concentration of fermentation inhibitors in the feed solution at a
512 steady state by only partially rejecting the inhibitors. The increase of sugar concentration and
513 ratio of sugar to fermentation inhibitors resulted in a higher yield of ethanol from fermentation,
514 with a yield of 18 g/L achieved as compared to 4.83 g/L with liquid fraction without
515 concentration process. These results show that FO can be incorporated prior to the fermentation
516 process to concentrate the sugar content and increase the bioethanol production efficiency.

517

518 A similar concept has also been applied to the recovery of succinic acid from the fermentation
519 broth. Succinic acid serves as precursor or starting material for many industrial valuable

520 products, such as for food, pharmaceuticals, green solvent and biodegradable plastics [83].
 521 Conventionally, succinic acid is synthesized through a chemical process using non-renewable
 522 materials (liquefied petroleum gas or petroleum oil). This synthetic approach and the starting
 523 materials are not environmentally friendly [84]. Hence, the sustainable production of succinic
 524 acid through the use of fermentation-based route was developed to harvest the succinic acid
 525 from easily available raw materials and using a less-hazardous synthesis process. Though
 526 fermentation can produce succinic acid, its concentration is too low for cost-effective extraction
 527 of succinic acid from the broth. In this case, FO membrane process was integrated prior the
 528 crystallization process to concentrate the succinic acid such that the concentration was suitable
 529 for crystallization to take place (Fig. 4) [85]. It was reported that FO managed to concentrate
 530 the succinic acid present in the real fermentation broth from 28.88 g/L to 111.26 g/L, with the
 531 retention of succinic acid in the feed solution as high as 99%. The concentrated fermentation
 532 broth was then crystallized to obtain succinic acid crystals, with the purity and yield recorded
 533 at 90.52% and 67.09%, respectively. Without FO concentration, none of the succinic acid
 534 crystals was found due to the low concentration and presence of impurities. Hence, the findings
 535 indicated that the FO process can help to materialize the sustainable production of succinic acid
 536 by concentrating the solution to the level suitable for crystallization process.



537

538 **Fig. 4.** Integrated FO-crystallizer for the purification of succinic acid from fermentation broth

539 (adapted from [85]).

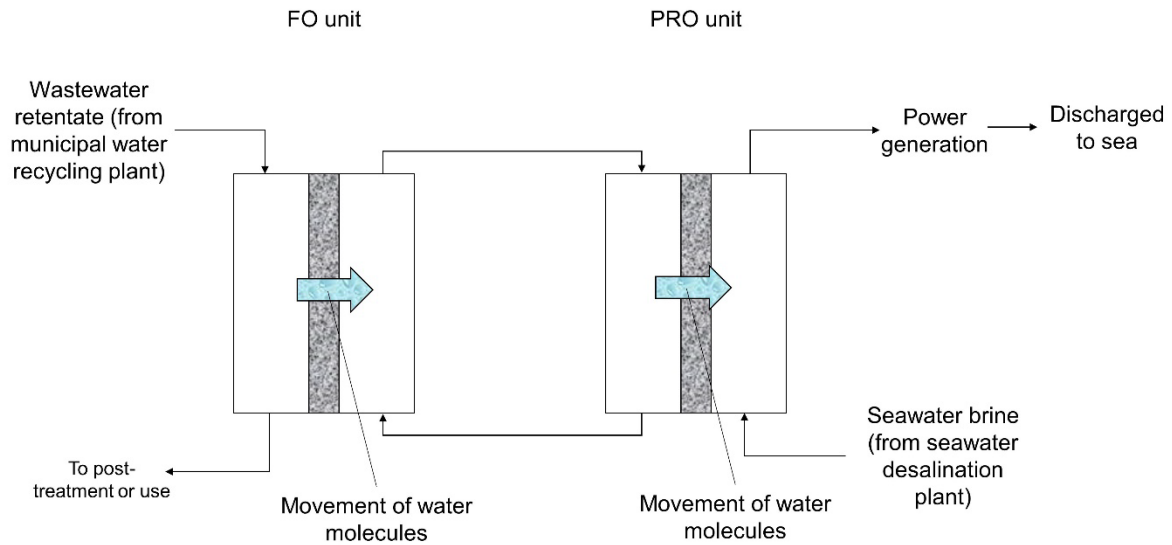
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541 Energy Generation and Resources Recovery

542 The FO membrane process has also found a potential role in energy generation by enhancing
543 the performance of renewable energy production through methane (biogas). One typical
544 integrated process is the combination of FO with anaerobic digestion (as in the form of MBR)
545 where FO helps to prepare the feed solution at optimal conditions for biogas production. The
546 FO process in OMBR extracted water from the bioreactor and at the same time led to the
547 concentration of solid contents in the bioreactor [40]. With more concentrated solid contents,
548 the biodegradation of organic contaminants would also be enhanced. Consequently, the
549 increase of bacterial activity also led to the rise of biogas production.

550

551 Another emerging technology for renewable energy production is through pressure retarded
552 osmosis (PRO) process. PRO utilizes the movement of water from low-salinity feed solution
553 across a membrane to a high-salinity draw solution against a hydraulic pressure for the
554 harvesting of renewable salinity-gradient energy [86]. Despite the great potential shown by
555 PRO in generating energy, membrane fouling still remains as one of the most challenging
556 issues prohibiting the commercial application of PRO technology. To alleviate the membrane
557 fouling issue, Cheng et al. (2018) have proposed to install FO as a pretreatment step prior to
558 the PRO process (Fig. 5) [87]. In this context, wastewater retentate from a municipal water
559 recycling plant was used as the feed solution while the draw solution was NaCl solution. Upon
560 dilution, the draw solution would be sent to the PRO system as feed while seawater brine was
561 used as the draw solution. In this operating mode, direct contact of wastewater with the PRO
562 membrane was prevented, and subsequently the issue of PRO membrane fouling could be
563 reduced.



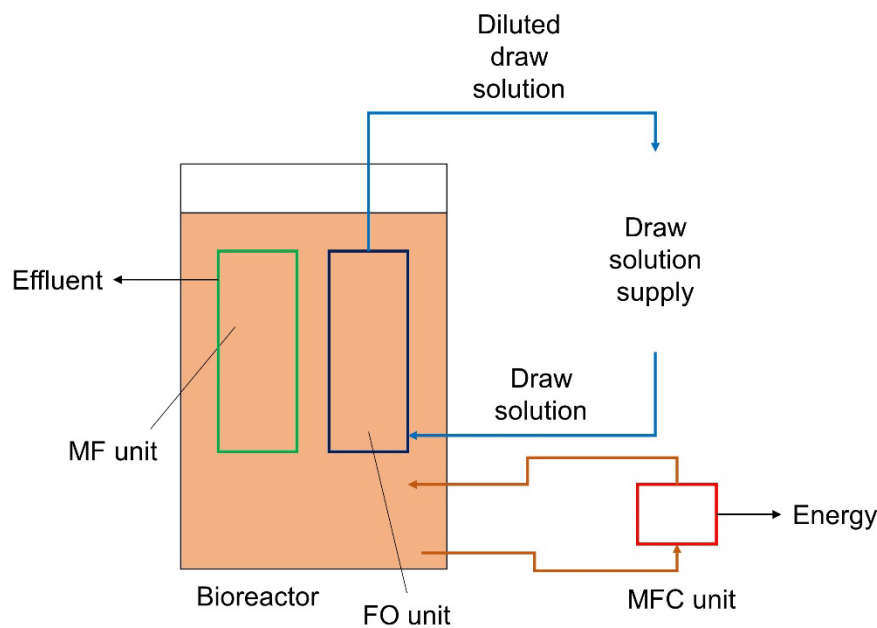
564

565 **Fig. 5.** Integrated FO-PRO process for power generation (adapted from [87]).

566

567 Bioelectrochemical systems such as microbial fuel cells and microbial electrolysis cells have
 568 emerged as one of the multipurpose processes for renewable energy production and wastewater
 569 treatment. The concept is developed where the microorganism in the anode of the cells will
 570 oxidize the organic substances present in the wastewater (biodegradation of wastewater), and
 571 the generated electrons can be used to produce electricity [88]. However, bioelectrochemical
 572 systems encounter several limitations for commercial applications, such as low electricity
 573 production and the treated water requires further treatment before it can be safely discharged
 574 [89]. To resolve these issues, the integration of a bioelectrochemical process with FO was
 575 explored. Liu et al. (2017) have shown that by integrating microbial fuel cells with anaerobic
 576 acidification and an FO membrane process, the bio-electricity production and clean water
 577 recovery for low-strength wastewater have been successfully enhanced [90]. The improvement
 578 of performance was attributed to the role played by FO process where it concentrated the
 579 ethanol and acetic acids (produced through anaerobic acidification process) in the bioreactor
 580 (as shown in Fig. 6), preparing the solution easier to be used by the exoelectrogens to produce
 581 electricity based on the fact that the simple substrates were more easily utilized for power

582 generation [91]. Another factor that contributed to enhanced electricity production was the
 583 controlled salt concentration in the bioreactor. MF membrane process was installed to
 584 consistently draw out the solution in the bioreactor to maintain a healthy salt concentration for
 585 the growth of microorganism and electricity production. The extracted effluent possessed a
 586 good quality with more than 97% removal of organic matters and total phosphorus, which could
 587 be used for toilet-flushing.



588

589 **Fig. 6.** Integrated OMBR-MFC for simultaneous wastewater treatment and bioenergy
 590 generation (adapted from [90]).

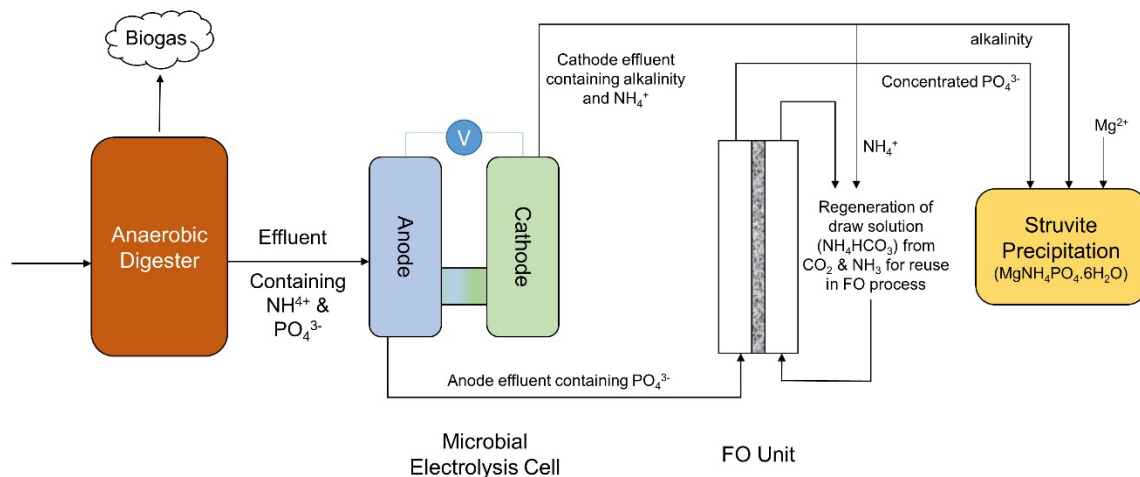
591

592 Other than energy recovery, integrated FO process is mostly associated with water recovery.
 593 However, unlike conventional pressurized membrane processes, the clean water is being
 594 recovered through another process during the regeneration of draw solution, where the FO
 595 process acts like a medium, extracting and transferring the clean water from feed to draw
 596 solutions. Plentiful of articles for water recovery through the regeneration of draw solution in
 597 integrated FO process have been reported, where the clean water can be extracted from various
 598 feed water (e.g. sewage, produced water, human urine, coal mine wastewater, etc.) and

600 recovered from different draw solution regeneration technologies (mainly membrane-based
 601 such as NF, MD, and RO) [60–67,69]. Since the details of these integrated FO processes have
 602 already been discussed in the previous section, and regeneration of draw solution will be
 603 discussed in the following section, the readers are advised to refer to the cited references for
 604 further information on water recovery through integrated FO processes.

605

606 Apart from recovering the water and energy resources in wastewater sources, integrated FO
 607 process can also be employed for nutrients recovery. The FO process has the potential to enrich
 608 the ammonium and orthophosphate, which are the key constituents present in the digested
 609 sludge centrate for struvite precipitation [92]. The elevated concentration of ammonium and
 610 orthophosphate will enhance the product yield of struvite. Zou et al. (2017) incorporated FO
 611 with microbial electrolysis cells for the recovery of energy, nutrients, and water as shown in
 612 Fig. 7 [54]. The microbial electrolysis cells harvest the energy potential lies in the wastewater
 613 through its anode. On the other hand, FO process was responsible for the concentration of
 614 wastewater such that the phosphorus nutrient could be recovered easily through chemical
 615 precipitation. The water extracted from the wastewater would be recovered as clean water after
 616 the diluted draw solution was regenerated. This shows the versatility of FO as a concentration
 process in completing the recovery of energy-water-nutrient from wastewater.



617

618 **Fig. 7.** Schematic idea of integrated MEC-FO system for nutrient-energy-water recovery
619 (adapted from [54]).

620

621 **Regeneration of Draw Solution**

622 FO process will generate two streams, concentrated feed and diluted draw solutions, where the
623 final product is determined by the purpose of having the concentration-dilution process. On
624 one hand, the desired product will be the concentrated or diluted streams. On the other hand,
625 the aim of the FO process is to extract and recover the clean water in the feed solution. As the
626 product of a simple FO system is not pure water, but rather the water is trapped in the diluted
627 draw solution, to obtain a pure water product FO needs to be part of an integrated process with
628 a second step aimed at both re-concentrating the draw solution and producing a pure water
629 product. The exception to this is in applications where the primary product is a concentrated
630 feed and/or where the draw solute has been chosen where reconcentration is not required, such
631 as seawater [93], fertiliser solutions which can be added to irrigation water [94–98], or
632 lignosulfonate which can be applied to crop soils as a conditioner [99]. The majority of draw
633 solution regeneration systems which have been investigated in the laboratory can be broadly
634 divided into the categories of: pressure-driven filtration; thermally driven systems; magnetic
635 recovery; electrolytic recovery; and precipitation based systems. Depending on the types of
636 draw solution, FO process will be integrated with the corresponding draw solution regeneration
637 process.

638

639 In cases where draw solution does not require regeneration, the associated costs consist merely
640 of pumping, storage, and other assorted costs depending on the situation used. For the FO
641 process itself, energy costs calculated by McGinnis and Elimelech was approximately 0.56

642 kWh/m³ for seawater desalination using an ammonia-CO₂ based draw solute system, compared
643 with an estimated 1.5 kWh/m³ minimum energy requirement for seawater RO [100,101].

644

645 Pressure-driven Filtration Processes

646 Membrane filtration processes, such as RO, NF, and UF have been investigated extensively for
647 the regeneration of diluted draw solutions. Whilst these systems are capable of treating a wide
648 range of feed waters directly, in this case the FO is being utilised as a low fouling primary
649 treatment, with the more fouling prone pressure-driven system being exposed to a relatively
650 simple and low fouling draw solution [102,103]. For instance, a study of a hybrid FO-RO
651 systems concluded that due to the relatively low water flux of the FO step, and consequent high
652 specific energy costs when including the RO step, hybrid FO-RO systems are best applied
653 when using feed waters with high fouling propensity [104]. When FO is applicable and
654 monovalent salts are the chosen draw solutes, RO is an attractive recovery technology due its
655 high salt rejection.

656

657 Yangali-Quintanilla et al. (2011) discovered that energy consumption for a hybrid FO-RO
658 desalination process with a low-pressure RO step was half that of a conventional high-pressure
659 RO process for the same feed water [14]. The authors cost analysis demonstrated that FO-RO
660 systems are potentially more cost-effective than desalination using RO alone but only when
661 high flux rates for the FO can be achieved (above 5.5 L/m².h). This threshold was even higher
662 when a low-pressure RO system with UF pre-treatment was the comparator (10.5 L/m².h).

663

664 Cath et al. (2010) developed a process they termed osmotic dilution, which used a seawater
665 draw solution to dewater wastewater [105]. The diluted seawater was then used as a feed for
666 brackish RO, for clean water production. This allowed simultaneous dewatering of wastewater

667 and seawater dilution. An estimated 63% of water was recovered from the wastewater source
668 as a potable product, with the RO step being lower cost than desalinating seawater directly.
669 Consequently, not only the RO process extracted water from the diluted seawater but also
670 recovered the clean water that has been pulled from the wastewater through FO process.

671

672 NF and UF are attractive recovery steps due to their higher flux rates for a given pressure than
673 RO, but their higher molecular weight cut-offs make them unsuitable for recovery of draw
674 solution consists of monovalent salts. Tan and Ng studied NF draw recovery process for $MgCl_2$,
675 $MgSO_4$, Na_2SO_4 and ethanol [106]. They reported high flux rates potentially achievable for the
676 combined ($10 \text{ L/m}^2\cdot\text{h}$) and high rejection (97.4%), with a double pass of NF needed to meet
677 WHO standards for potable water. Other researchers desalinated brackish water using a hybrid
678 FO-NF system with $NaSO_4$ and $MgSO_4$ as draw solutes [29]. They reported lower irreversible
679 membrane fouling compared with conventional RO treatment of identical feedwater.

680

681 The high flux rates and low specific energy costs associated with UF make it an attractive
682 second step when draw solutes are in the colloidal size range [107,108]. For instance, Ge et al.
683 (2012) used UF to re-concentrate poly-acrylic acid (PAA) draw agent and achieved a rejection
684 of 98.5 to >99%, depending on the molecular weight [109]. Nonetheless, this rejection rate still
685 leads to a noticeable drop in FO flux after multiple cycles due to loss of solute and consequently
686 lower draw solution osmotic potential. However, as was pointed out by Shaffer and co-workers,
687 any good recovery step must necessarily make a return to the same original osmotic pressure
688 and as such the minimum energy requirements are the same regardless of whether the second
689 step is RO, NF or UF [30].

690

691 Temperature-driven systems

692 The very first applications of FO used volatile draw solutes which allowed temperature based
693 recovery to be used. Research has included decomposition into gases, such as when ammonium
694 bicarbonate or sulfur dioxide are used [101,110–113]. Another technique which has been
695 demonstrated was in the use of switchable polarity solvents. Stone et al. (2013) investigated
696 this type of regeneration process using ternary mixtures of primary amines, CO₂, and water
697 [114]. The diluted draw solution was gently heated with application of oxygen or nitrogen gas,
698 which caused the mixture to undergo a phase transition. Solid amines precipitates could then
699 be easily removed, with remaining traces removed using RO. Further research found such a
700 process combined with FO to be favorable, in terms of energy usage compared with
701 conventional seawater RO [115]. Similar concept has also been demonstrated in a pilot-tested
702 FO-membrane brine concentrator plant [116]. The draw solution used in this pilot plant was
703 NH₃/CO₂ (a mixture of thermolytic ionic solutes) solution, where upon diluted would be
704 directed to a distillation column to vaporize the draw solutes, which subsequently condensed
705 to regain the draw solution for reuse. It was reported that the integrated system could attain
706 water recovery of 64% from the produced water.

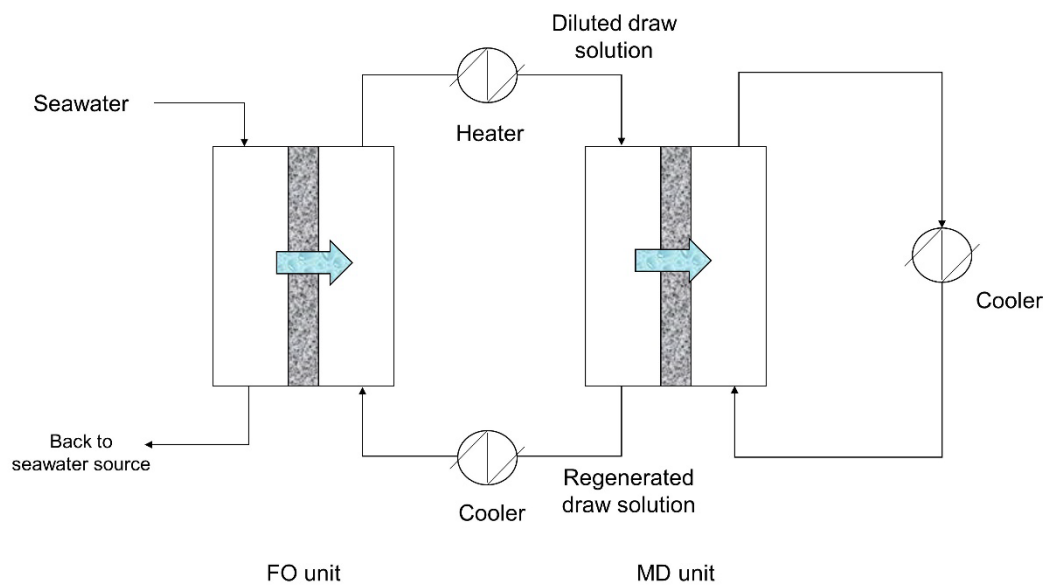
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708 Membrane distillation (MD) is another thermally driven process which has been explored as a
709 draw solution re-concentration process [92]. Yen et al. (2010) used an FO-MD hybrid process
710 using de novo designed 2-methylimidazole based organic compounds as draw solutes, with the
711 draw solution being continuously re-concentrated using MD [117]. They found that the flux
712 rates were more stable over time due to the maintenance of the draw solution at a high
713 concentration.

714

715 MD has also been combined with the use of temperature-sensitive polymers which undergo
716 solubility changes at increased temperatures, combined with filtration of the precipitate (Fig.

717 8) [118]. At the temperature above the low critical solution temperature of the draw solutes
 718 (heated before entering MD unit), it will agglomerate and lead to decreased osmotic pressure
 719 and thus higher water vapor pressure (subsequently enables the recovery of clean water).
 720 Thermo-responsive polymers have also been used to coat nanoparticle systems to allow re-
 721 dispersal of nanoparticle draw solutes which have been recovered using magnetic collection
 722 systems [119,120].



723

724 **Fig. 8.** Integrated FO-MD for seawater desalination and regeneration of draw solution (adapted
 725 from [118]).

726

727 The energy consumption of a hybrid FO-MD process for regenerating a thermos-responsive
 728 co-polymer draw solution system was investigated by Zhao et al. (2014) [118]. It was reported
 729 that 29 kWh/m³ was required, with the major contributor to the cost increase over pure FO
 730 being heating for the MD process. However, if a waste or free heat source is available this can
 731 be reduced considerably. For instance, Suwaileh et al. (2019) demonstrated that it is feasible to
 732 provide the heating for the MD process using solar collector systems, reducing the energy
 733 footprint for a hybrid FO-MD process to a significant extent [121].

734

735 Magnetic Recovery

736 Magnetic nanoparticles have been explored as potential draw agents in FO, which allows for
737 the possibility of reconcentration using magnetic collectors. Typically, these have used
738 magnetite nanoparticles coated with hydrophilic polymer brushes [122]. There are a number of
739 issues with the magnetic recovery of nanoparticles, predominantly the aggregation of these
740 particles, which ultimately leads to a loss in the osmotic potential of the nanoparticle
741 suspensions and decreased FO flux after reconcentration cycles. Ling and Chung used
742 ultrafiltration to separate magnetic nanoparticle agglomerates after particle collection, but with
743 the reduction in magnetic properties of the particles [123]. Other researchers have used
744 nanoparticles coated in environmentally responsive polymer brushes, to allow particle
745 dispersion through application of external stimuli such as magnetic or sunlight [120,124–126].

746

747 Razmjou et al. (2013) used thermally responsive hydrogels with entrapped magnetic
748 nanoparticles. This allowed water to be released using magnetically induced heating, which
749 was found to occur more evenly and at a greater rate than other forms of heating, releasing 53%
750 of bound water using magnetism compared with 7% from conventional heating [127].

751

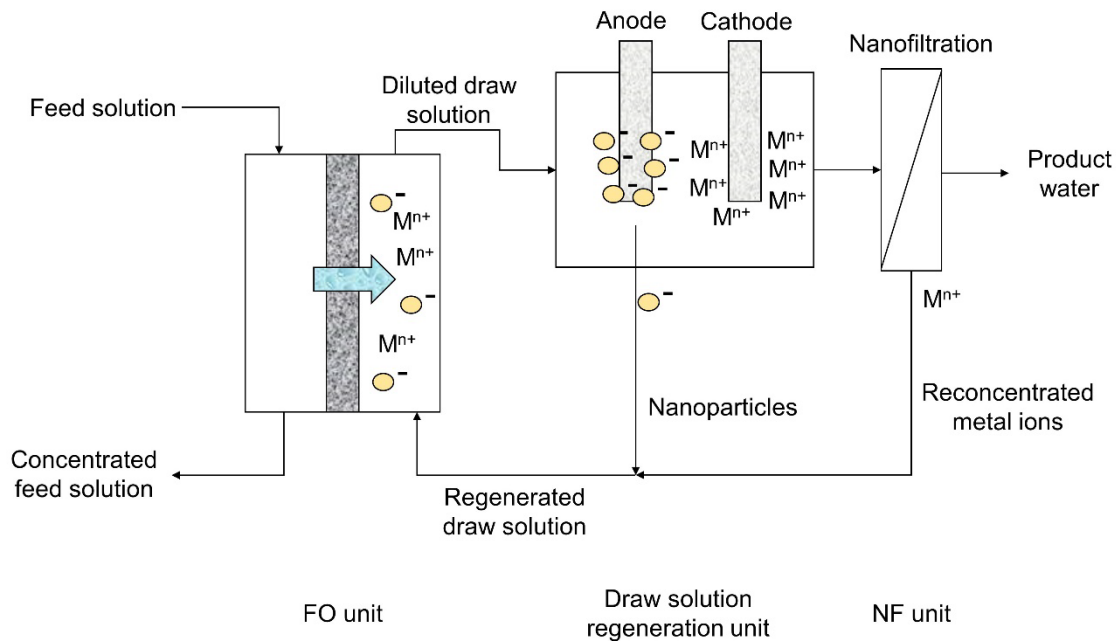
752 Ling et al. (2011) studied UF for recovery of super-hydrophilic magnetic nanoparticle draw
753 agents. It was reported that UF was a superior recovery method over the magnetic collection,
754 due to lack of particle agglomeration and associated osmotic potential loss [124].

755

756 Electrolytic Recovery

757 Ling and Chung observed that magnetite nanoparticles had high electrical conductivity, and
758 thus recovery using electrical fields is possible [125]. As shown in Fig. 9, particle accumulated
759 on the anode placed in the draw solution tank allowing easy recovery, with metal ions left in

760 solution recovered using NF. The alkaline metal ion solution was then used to re-disperse the
 761 nanoparticles. Water flux was maintained after repeated regeneration cycles. However, it is not
 762 clear what advantage such a system would have in terms of energy costs and after scale-up
 763 when compared with simple re-concentration of draw solution using NF alone, without the
 764 electrolysis step.



765

766 **Fig. 9.** Regeneration of draw solution via integrated electrical fields and NF membrane process
 767 (adapted from [125]).

768

769 Electrodialysis has also been investigated for the concentration of diammonium phosphate
 770 (DAP) draw solute which had leaked into the feed water during FO treatment of wastewater
 771 [128]. DAP recovery was reported to be 96.6%, with the FO-ED system operating at 0.72
 772 kWh/m³ when using pure water feed. However, when using actual treated wastewater as a feed
 773 solution to the FO process intense fouling was observed, which required repeated cleaning
 774 steps.

775

776 Precipitation of Draw Solute

777 Another method which has been explored to allow recovery and re-use of draw solutes is
778 through precipitating systems. For instance, an $\text{Al}_2(\text{SO}_4)_3$ draw solution has been used [34],
779 with the addition of calcium hydroxide causing the $\text{Al}_2(\text{SO}_4)_3$ to precipitate before recovery
780 either by sedimentation or filtration [129]. Other precipitating draw solutes, such as MgSO_4 or
781 CuSO_4 have also been investigated using similar processes [130,131]. In the case of CuSO_4 , it
782 was found that flux rates ($3.6 \text{ L/m}^3\cdot\text{h}$) were obtained for brackish feed water, but osmotic
783 pressures were not high enough to desalinate seawater. In addition, concentration polarization
784 effects were significant. However, precipitation of the CuSO_4 using barium sulphate in a
785 metathesis was capable of delivering pure water as a product without further polishing needed
786 [130].

787

788 **FO Fouling Mitigation**

789 It has been generally reported that FO demonstrates a much lower fouling propensity and
790 higher fouling reversibility than RO, which could be attributed to the lack of applied hydraulic
791 pressure [103,132]. These properties have enabled FO to be used for the handling of various
792 low-quality water sources, including landfill leachate, municipal wastewater, leather industry
793 effluent, coal mine wastewater, produced water, and anaerobic digestate [39,48,57,60–67,133].
794 However, fouling is still prevalent in the FO process as the phenomenon of flux decline can be
795 frequently seen in the published results. Fouling in FO is normally associated with the
796 deposition of suspended impurities on the membrane surface that block the passage of water
797 and leads to concentration polarization [134]. Fouling will cripple the capability of the
798 membrane process (flux and retention of impurities) and incur additional costs associated with
799 cleaning for the restoration of membrane performance and membrane replacement expenses
800 [135]. Hence, to alleviate the issue of membrane fouling, pretreatment processes can be

801 integrated prior to the FO process, as what has been frequently practiced to minimize the
802 fouling issues in other membrane processes.

803

804 The concentration of synthetic greywater using a hollow fiber thin-film composite FO
805 membrane process demonstrated a substantial flux decline in the range 20-40%, which could
806 be attributed to the accumulation of protein on the membrane surface [136]. The formation of
807 foulant layer on the membrane surface induced concentration polarization and increased the
808 mass transfer resistance of water, which led to a decrease in the membrane flux. With the
809 adoption of ferric flocculant prior to the FO process, the normalized flux decline was at a
810 marginal 3% only, as compared to the flux decline without any pretreatment at about 40%.
811 Moreover, the recovery of the FO flux after the concentration of greywater was 100% where
812 the foulant could be removed simply by soaking the membrane in deionized water. This
813 signified the role of the flocculation process in removing some of the main contaminants (96%
814 of casein) in the synthetic greywater. Subsequently, the FO membrane was less exposed to the
815 contaminants that could block its surface for water passage. A similar finding was also reported
816 by Hawari et al. (2018) where the FO membrane flux was approximately 50% higher when
817 subjected to the concentration of pretreated dewatered construction water (through multimedia
818 filtration) [137]. The significant increase in flux was due to the removal of large amounts of
819 suspended solids and turbidity (impurities) by the multimedia filtration pretreatment process,
820 reducing the turbidity and total suspended solids from 300 NTU and 325 ppm to 24 NTU and
821 21 ppm, respectively.

822

823 Fracking wastewater is highly saline water that contains different types of inorganic salts,
824 dissolved organic compounds, oil, and sand [138]. It is high-strength wastewater that must be
825 handled properly for the viability of the fracking industry, human health, and environment.

826 Directly applying FO process to concentrate the fracking wastewater is not economically viable
827 as the impurities will easily foul and damage the membrane. Hence, pretreatment is required
828 to improve the integrity of FO process and its life expectancy by removing these compounds.
829 Pretreatment with MF membrane has proved to be efficient in the removal of impurities present
830 in fracking wastewater where it was reported the MF membrane removed nearly 52% of TOC
831 and 98.5% of turbidity [139]. The pretreated fracking wastewater was then channeled to the
832 FO process as feed solution. Comparison of FO flux patterns with raw and pretreated fracking
833 wastewater showed that the latter achieved much lower flux decline (14%) as compared to the
834 former (55%). This observation could be explained by the presence of MF pretreatment where
835 a large portion of the foulants have been removed by MF. Similar trend of finding has also
836 been reported where electrocoagulation was adopted as pretreatment to reduce up to 78% and
837 95% of TOC and turbidity in hydraulic fracturing produced water, respectively [140]. Without
838 pretreatment, the FO membrane would be exposed to the impurities that have high potential to
839 block the membrane surface.

840

841 Apart from chemical precipitation and physical filtration as the pretreatment processes,
842 advanced oxidation process has also been integrated with FO for the treatment of anaerobically
843 treated dairy effluent [141]. The advanced oxidation process is a technology that degrades the
844 organic compounds present in the water sources [142]. The incorporation of an advanced
845 oxidation process could help to eliminate the organic compounds in the wastewater and
846 contribute to the alleviation of membrane fouling. For instance, Pramanik et al. (2019)
847 incorporated ultraviolet and persulfate as pretreatment prior to the FO process for anaerobically
848 treated dairy effluent [141]. The pretreatment process significantly reduced the concentration
849 of biopolymers, humics, and other organics in the effluent, prompting the FO process to acquire
850 higher water flux and water recovery. This could be attributed to the change in form of the

851 compounds. Originally, these compounds possessed high molecular weight and were
852 hydrophobic in nature, which meant that they had a high tendency to adhere to the membrane
853 surface. The pretreatment process degraded the compounds from high to low molecular weight
854 hydrophilic molecules, effectively minimizing the build-up of organic compounds on the FO
855 membrane surface.

856

857 With the growing amount of municipal solid waste being disposed into landfills, the production
858 of undesirable landfill leachate containing a range of persistent contaminants has also got more
859 serious [143]. It has been reported that the FO membrane process could be employed to
860 concentrate the landfill leachate though the process suffered from membrane fouling issues
861 [144]. In a study conducted by Aftab et al. (2019), activated carbon (AC) and biochar (BC)
862 have been integrated with FO process as pretreatment to alleviate the membrane fouling issues
863 [133]. The addition of these adsorbents has resulted in enhancement in terms of flux, flux
864 recovery, and membrane resistance, especially the experimental set with AC. These
865 improvements could be due to the adsorptive property of AC that could capture the impurities
866 in the leachate, which possessed the potential to foul and degrade the performance of FO
867 membrane process. With the optimal dosage of AC, the irreversible membrane resistance has
868 been reduced to the level nearly equal to the virgin FO membrane (notable reduction in
869 irreversible fouling). Hence, this shows that the removal of impurities in the water sources
870 could help to alleviate the membrane fouling issues and enable the FO process to concentrate
871 the feed water.

872

873 Mitigation and prevention of FO membrane fouling can also be achieved indirectly through the
874 design of hybrid FO process. For instance, when the biological treatment process of OMBR
875 has been modified into biofilm or entrapped cells forms, the fouling propensity of FO process

876 has also been minimized [48,49]. When the bacteria grew in a fixed place (biofilm and
877 polymeric matrix), the amount of free-form bacteria (suspended) in the bioreactor had also
878 been reduced. Furthermore, the continuous draw-out of wastewater from the bioreactor helped
879 to remove a portion of the dispersed cells. The change in the bioreactor form reduced the
880 presence of suspended cells and subsequently minimizing the deposition of foulants on the FO
881 membrane.

882

883 **Future Challenges**

884 Even though the potential of FO has been proven through integrated/hybrid processes, there
885 are some areas of studies that need to be further investigated before the concept of
886 integrated/hybrid FO process can be commercially implemented.

- 887 • Most of the performance data of integrated/hybrid FO process have been collected from
888 lab-scale testing. There is still a lack of comprehensive data from pilot-scale or real
889 application of integrated/hybrid FO process to convince the industry to adopt this concept
890 in their process. Though pilot-tested results of FO in various wastewater treatment, for
891 instance oil and gas wastewater, showed that the FO process could recover up to 85% of
892 water for reuse, the case studies did not provide detailed information as in the overall cost
893 of the whole treatment process (including draw solution regeneration) [145]. Furthermore,
894 the flux decline appeared to be significant, which indicated the need of frequent cleaning
895 [6,68,146]. Though it was claimed to be easily cleaned, the impacts of membrane fouling
896 and cleaning on the overall performance and cost remain unexplored/unreported.
- 897 • Though the reported performance of integrated/hybrid FO processes are quite encouraging,
898 the associated cost has often been left out with no data on the improvement of overall
899 expenditure. For instance, pretreatment process installed prior to FO process can help to
900 alleviate the membrane fouling issue, but benefits in term of cost benchmarking (expenses

901 arising from the installation of pretreatment versus the gain from less frequent cleaning
902 and longer membrane lifespan) has never been properly documented.

- 903 • Feasibility of long-term operation of integrated/hybrid FO process has rarely been reported.
904 As the FO membrane flux is considerably low, the question is whether the FO can produce
905 sufficient flux to sustain the whole integrated/hybrid process for long-term continuous
906 operation. This poses challenges to the membrane community in synthesizing FO
907 membrane with great capability in terms of flux, retention of impurities, and long lifespan.
908 Also, suitable low-cost draw solutes with ease of regeneration are vital for the long-term
909 operation of integrated/hybrid FO process.
- 910 • Sustainability of the integrated/hybrid FO process should be benchmarked against the
911 conventional or competitive alternative processes. As the world is aiming to achieve
912 sustainable development, the insight of the associated environmental impacts with the
913 implementation of integrated/hybrid FO process should be explored. This information may
914 provide another side of the story on the attractiveness of integrated/hybrid FO process.
- 915 • The success of integrated/hybrid FO process is also highly relying on the quality of the FO
916 membrane. Though remarkable advancement has been achieved in membrane fabrications,
917 the commercial market still lacks of FO membranes that could support industrial scale
918 application of FO process. Challenges remain in the aspect of control over membrane
919 properties (such as thickness, porosity, pore structures, water permeability, selectivity, and
920 antifouling) that will decide the practicality of up-scaled integrated/hybrid FO process in
921 terms of productivity (flux) and membrane fouling. Incorporation of nanoparticles seem
922 to be able to improve the membrane properties, yet it is challenged with the difficulties in
923 term of leakage, cost, and mass production of the FO membrane incorporated with
924 nanoparticles.

925 • Another hindrance for widespread application of integrated/hybrid FO process is the
926 availability of draw solute which can generate high osmotic pressure yet with minimum
927 reverse solute flux and at the same time can be easily regenerated (minimal energy
928 consumption). Though a significant amount of work has been done on the exploration of
929 draw solute (type and regeneration) for FO process, the ideal draw solute for upscaling
930 application remains absent. Existing draw solute is economic infeasible, either the
931 material is costly or the cost associated with regeneration is too high.

932

933 Of all the challenges mentioned above, almost all are related to the economic aspect of FO
934 process. The economic feasibility of integrated/hybrid FO process remains a disputed topic as
935 comprehensive cost analysis for real application has been limited. Different views of economic
936 feasibility have been reported in the literature, including the references discussed in the previous
937 sections. For instance, the FO process utilizing fertilizer as draw solution and operated at
938 flowrate of 400 mL/min consumed 0.396 kWh/m³ of energy, which was considered lower than
939 the conventional activated sludge plant (0.5647 kWh/m³) and conventional MBR processes
940 (1.0465 kWh/m³) [147–150]. However, the finding was limited to lab-scale testing using low
941 salinity brackish water (5000 ppm NaCl) and without the need of draw solution regeneration,
942 where the relative size of an actual plant receiving real sample might give a different
943 performance in the long run. Furthermore, the concentration polarization issue was apparent in
944 the testing, as reflected by the FO flux decline. This indicates the possibility of higher
945 expenditure for long time operation in real application.

946

947 The increasingly popular integrated/hybrid FO-MBR process for wastewater reclamation
948 though possesses attractive performance, economic analysis revealed the opposite finding.
949 Based on the SEC calculated, the integrated FO-MBR recorded up to seven times higher value

950 than that for classical RO process (0.29-1.2 kWh/m³) [6,151]. In another pilot-scale
951 demonstration plant, the integrated FO-NF process was treating MBR effluent for water
952 recovery. The NF process was used to regenerate the draw solution while extracting clean water.
953 The cost of product water was approximately 0.96 €/m³, which was twice the cost for
954 desalination (UF-RO) as tertiary treatment [64]. The much higher cost could be attributed to
955 the loss of draw solute (NF permeate and reverse solute flux) and energy consumption for the
956 NF process. Nonetheless, it was argued that the cost of a large-scale integrated FO-NF process
957 might be competitive as the typical UF-RO process for tertiary wastewater reclamation.

958

959 Despite there are positive simulation results supporting the economic feasibility of FO process
960 for integrated desalination process, there is no evidence from large-scale demonstrations that
961 integrated FO-RO process can consume less energy than the classical seawater RO desalination
962 process. Instead, it has been determined that integrated FO-RO can only energetically compete
963 with the RO desalination process at flux above 30 L/m³.h or associated recovery of more than
964 50% [6,152]. However, the integrated FO-RO desalination process could possibly attain
965 savings in energy if it was using secondary wastewater effluent as feed solution to dilute the
966 seawater (draw solution), as discussed in the previous section [14,16]. Alternatively, the cost
967 of the integrated FO process could be potentially reduced if the regeneration of draw solution
968 is not required, or the energy required could be derived from low-cost or renewable sources
969 such as solar energy or waste heat [118,121,150].

970

971 **Conclusions and Perspectives**

972 In general, the possibility of integrating and hybridizing FO membrane with other processes
973 enables the full utilization of FO capability in various applications. To sum up,
974 integrated/hybrid FO membrane processes have brought the following benefits:

- 975 • Dilution of seawater or brine minimizes the scaling issue in seawater RO desalination and
976 MSF desalination processes and potentially reduces the energy consumption due to lower
977 osmotic pressure of diluted seawater or brine.
- 978 • Enhancement of the quality of extracted water from MBR by preventing the impurities
979 from passing through to the draw solution side. The dewatering capability of FO helps to
980 maintain the characteristics of the wastewater in the bioreactor, making the conditions
981 suitable for optimal bacterial activity in degrading the organic impurities and producing
982 biogas (methane) as renewable energy.
- 983 • The modification on the bacterial growth mode in the bioreactor from suspended cells form
984 to attached growth (biofilm) or entrapped-cell form mitigates the organic fouling of FO
985 membrane in OMBR.
- 986 • Integration with other technologies such as coagulation, membrane, adsorption, and
987 electrochemical processes removes the total organic carbon and total suspended solids in
988 the wastewater. This helps to minimize the fouling propensity of FO membrane in
989 wastewater treatment process since these compounds could easily block and clog the
990 membrane.
- 991 • Integrated FO process could be an alternative concentration process for food and beverage
992 industries where the bioactive compounds are especially sensitive and vulnerable to heat.
993 The integrated FO process also converts the waste stream into valuable materials by
994 concentrating the valuable and useful compounds in the solution, or preparing the solution
995 suitable for subsequent downstream process.
- 996 • Concentrating the wastewater in electrochemical processes for more efficient energy
997 generation from microorganism and the recovery of phosphorus nutrient.

- 998 • Regeneration of draw solution through various approaches (pressure-driven filtration,
999 temperature-driven, magnetic recovery, electrolytic recovery, and precipitation) provides
1000 the FO an opportunity to be operated continuously and be applied in many applications.
- 1001 • Installing pretreatment processes prior to FO helps to mitigate the fouling issues associated
1002 with FO process. This ensures the FO process can be operated without severe flux decline
1003 and the membrane can be used for a longer period on top of less frequent of cleaning need.

1004

1005 Research on forward osmosis (FO) is attracting increasing interest due to its unique ability to
1006 provide an alternative mechanism to the other membrane processes especially for concentrating
1007 or diluting a solution using membranes. However, it is important that FO processes are
1008 integrated with other technologies in order to provide better process performance and cost
1009 saving. Various combinations of FO with other techniques have been reported especially for
1010 the purpose of process enhancement, draw solution regeneration, and pretreatment for FO
1011 fouling mitigation. These combinations have been shown to provide advantages in terms of
1012 reducing the membrane fouling propensity; preparing the solution suitable for subsequent
1013 value-added uses and production of renewable energy; lowering the costs associated with
1014 energy consumption; enhancing the quality of treated water; and enabling the continuous
1015 operation of FO through the regeneration of draw solution. There are many areas that still can
1016 be explored within these applications especially in terms of process optimization, large scale
1017 performance, economic assessment, and sustainable operations. The future challenges will be
1018 dependent on how FO can be hybridized or integrated in combination with other technologies
1019 to minimize its own shortcoming while enhancing the overall performance.

1020

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1025

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